

Field and Data Processing Methods for Developing Shear Modulus and Damping Properties Needed to Model Near-Surface Site Effects in Design Ground Motions

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2025 SCEC Shallow Earth Workshop

Palm Springs, California; 11 November 2025

A Letter from Sid

3rd Grader at Elsa England Elementary School in Austin, Texas

3-24-14

Dear Mr. Cox,

Thank you for the presentation about earthquakes. The presentation was really good! you are really lucky you got to meet the present. was it true or not? What are the things that can detect vibration called

again? my third option of job is a earth quake @ngin eare

It is a really cool job traveling around the world must be fun.

Sincerely,
sid



Founding Director: Utah Earthquake Engineering Center

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Science & Technology

USU Receives \$2.5M to Launch Earthquake Engineering Research Center

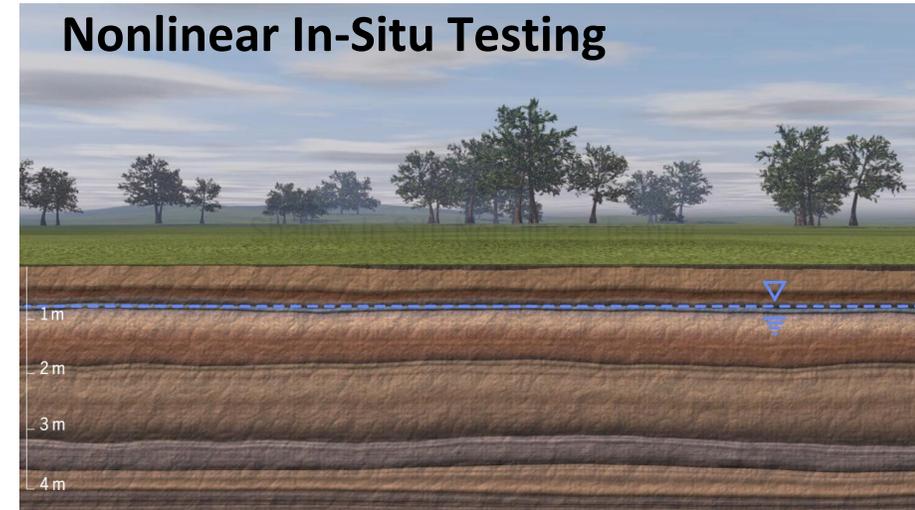
By Matt Jensen | March 16, 2023



2020 M5.7 Magna, Utah Earthquake



Co-PI of NHERI@UTexas NSF Center



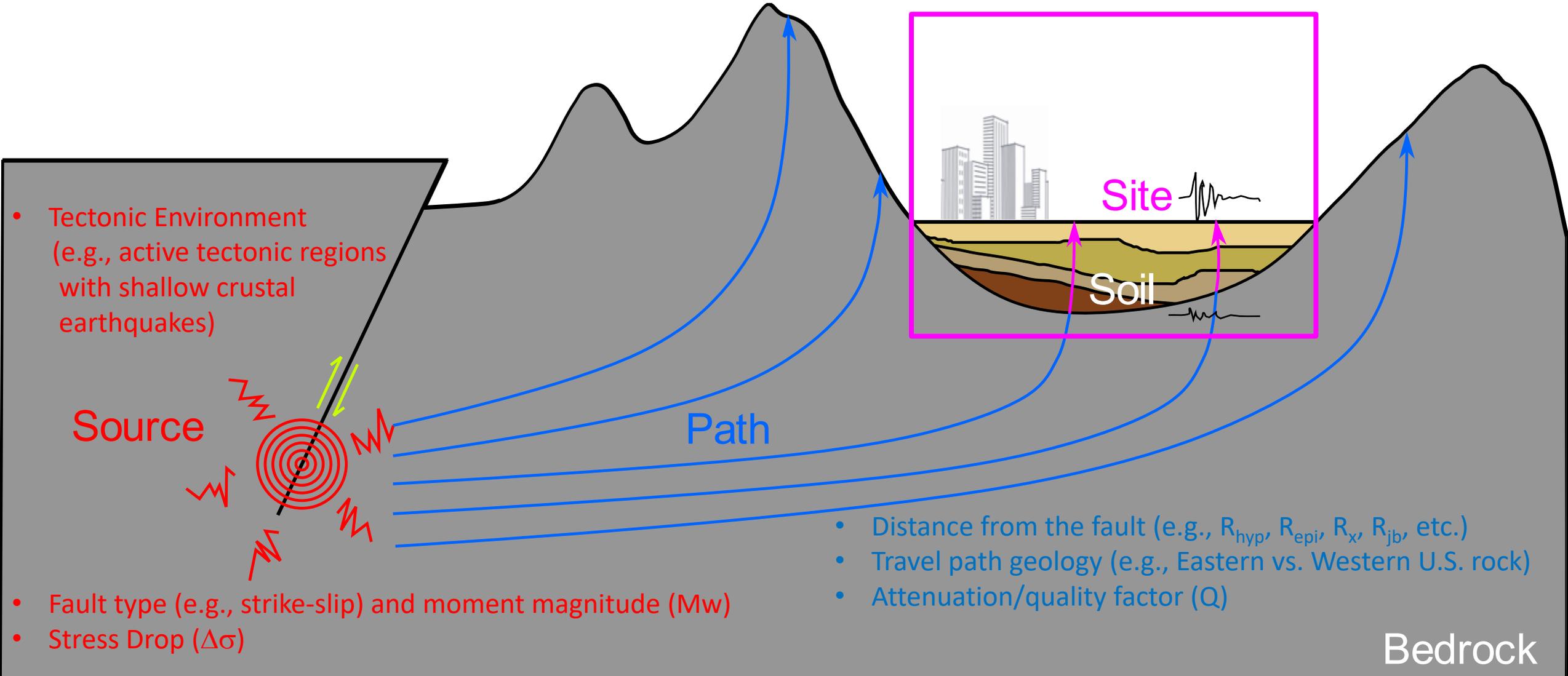
<https://utexas.designsafe-ci.org/>

Large, mobile dynamic shakers and instrumentation for natural hazards research



Background on Seismic Site Effects

You want to construct a new building. You need to determine what seismic forces the building will be designed to resist. What factors will influence the intensity and frequency content of the seismic ground motions used for design?

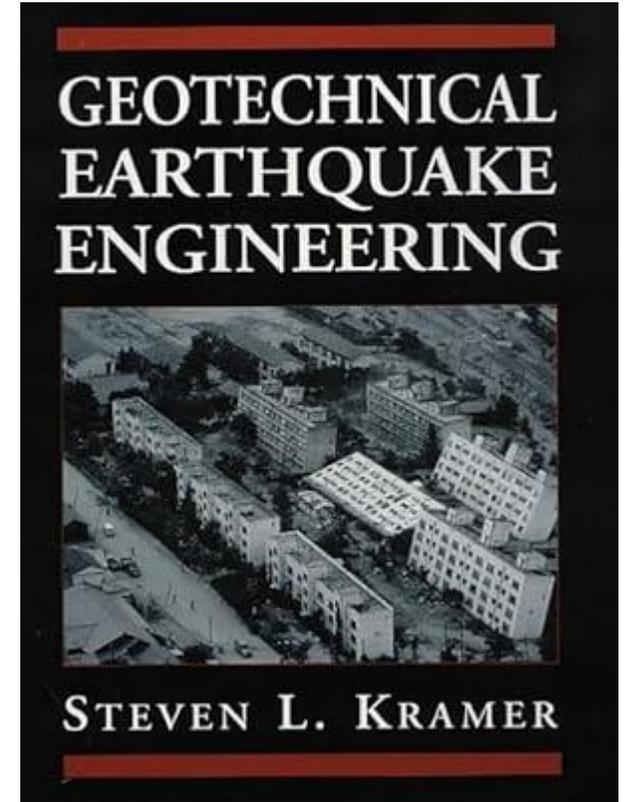


Background on Seismic Site Effects

You want to construct a new building. You need to determine what seismic forces the building will be designed to resist. What factors will influence the intensity and frequency content of the seismic ground motions used for design?

“Although seismic waves travel through rock over the overwhelming majority of their trip from the source of an earthquake to the ground surface, the final portion of that trip is often through soil, and the characteristics of the soil can greatly influence the nature of shaking at the ground surface. Since soil conditions often vary dramatically over short distances, levels of ground shaking can vary significantly within a small area.”

Kramer (1996)



Background on Seismic Site Effects

You want to construct a new building. You need to determine what seismic forces the building will be designed to resist. What factors will influence the intensity and frequency content of the seismic ground motions used for design?

... or perhaps stated more clearly

“The wise man built his house upon a rock...

and the foolish man built his house upon the sand...

and great was the fall of it.” Matthew 7: 24-27



Background on Seismic Site Effects

1985 Mexico City Earthquake (Mw 8.0)

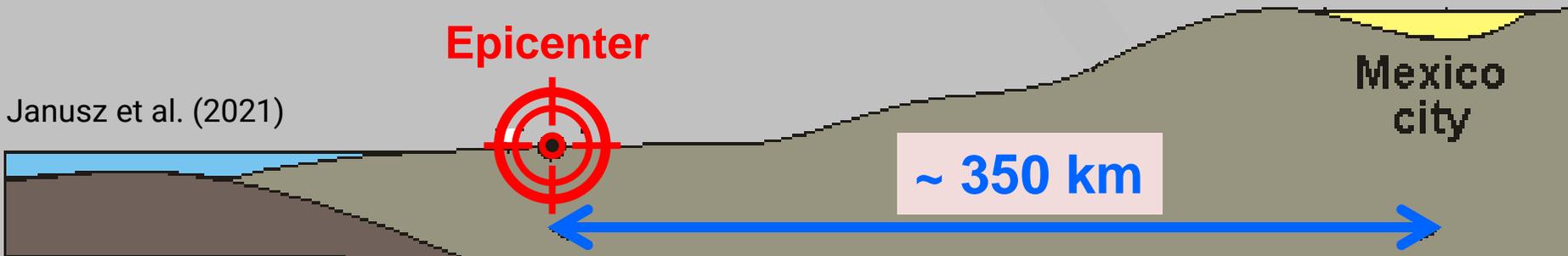
More than 400 buildings collapsed, and thousands more were damaged.

Majority of damaged buildings were 5 – 15 stories and were founded on soft lake-bed sediments (plastic clays)

~ 10,000 people lost their lives

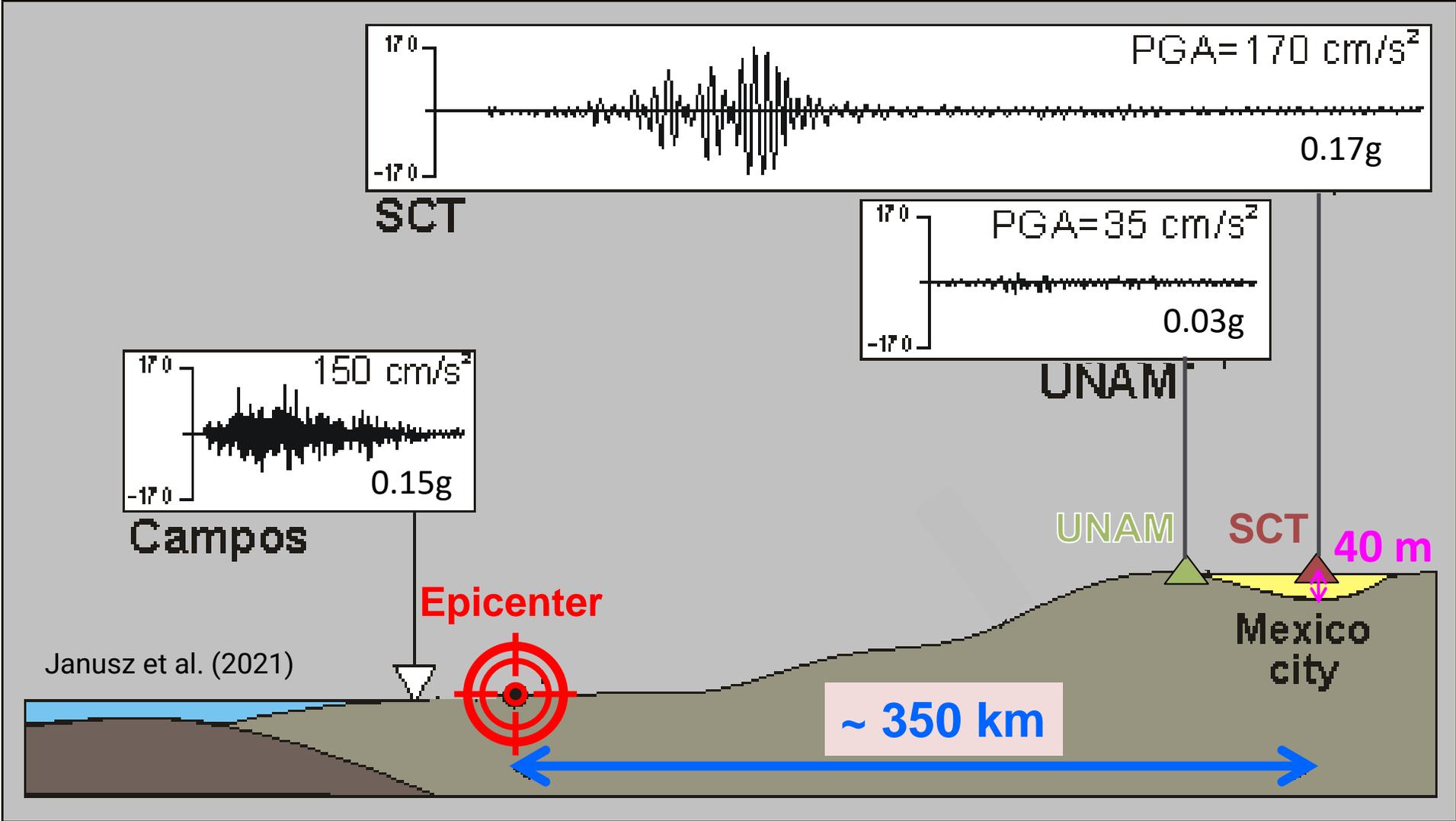


Soft clay deposits:
former Lake Texcoco



Background on Seismic Site Effects

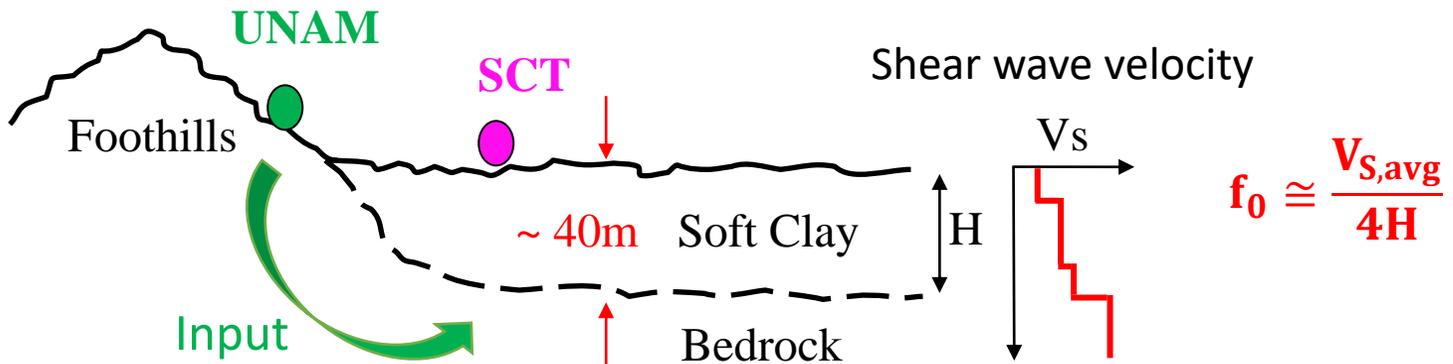
1985 Mexico City Earthquake (Mw 8.0)



Site Effects!

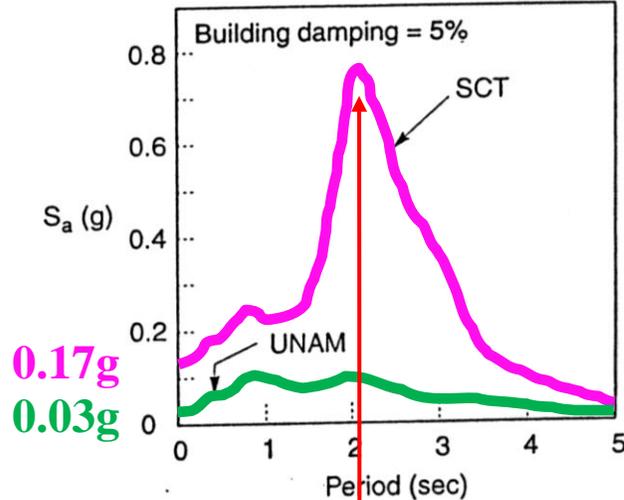
< 0.01% of travel path

Background on Seismic Site Effects



The importance of estimating f_0 when performing seismic site response cannot be over emphasized!

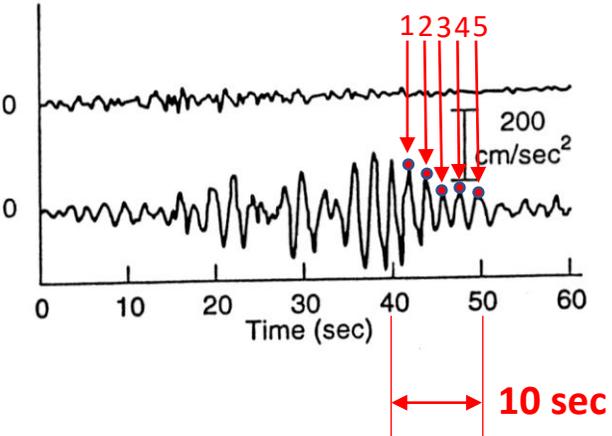
Spectral Acceleration



Predominant Period (T_p), or Fundamental Site Frequency (f_0)
 $f_0 = 1/T_p$



Recorded Ground Motions



$f = \frac{5 \text{ cycles}}{10 \text{ sec}} = 0.5 \text{ Hz}$
 $T = 1/f = 2.0 \text{ sec}$

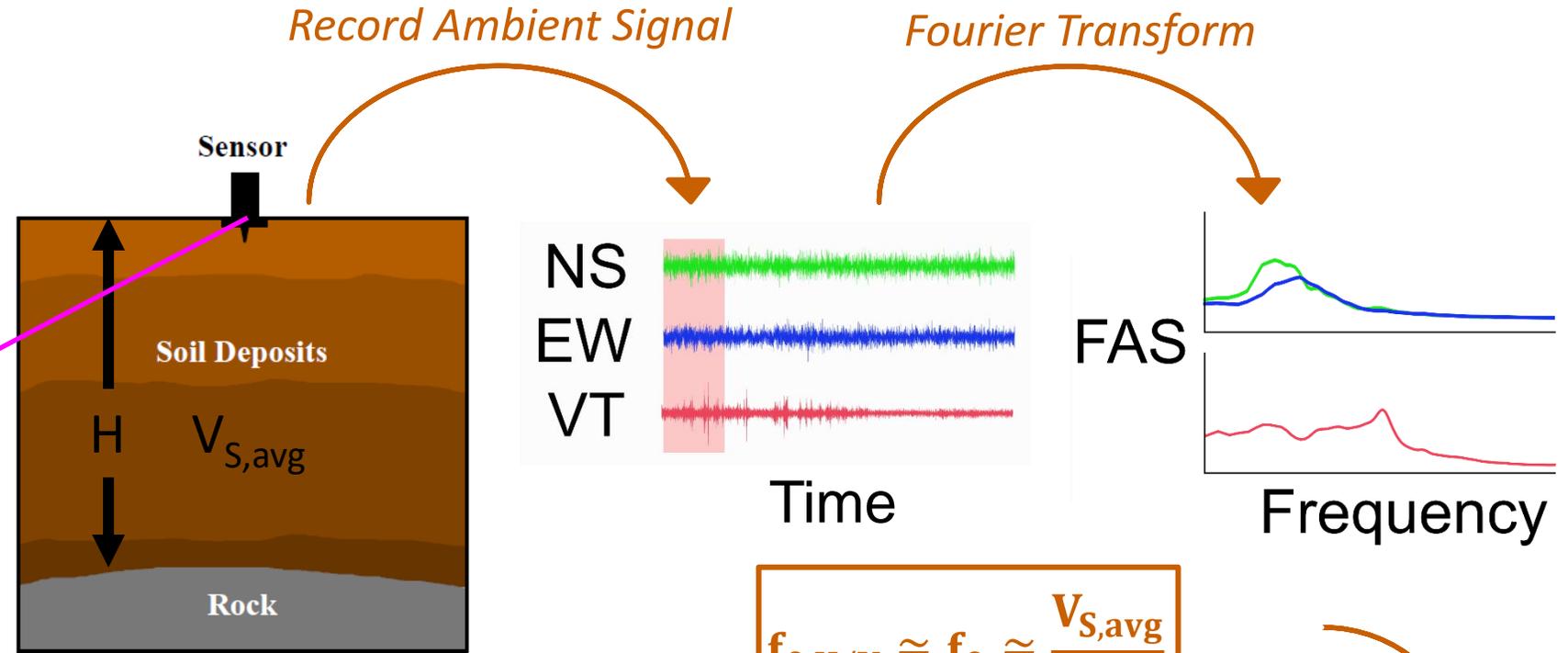
Stone et al. (1987)

An Aside on Measuring f_0 using HVSR of ambient noise measurements

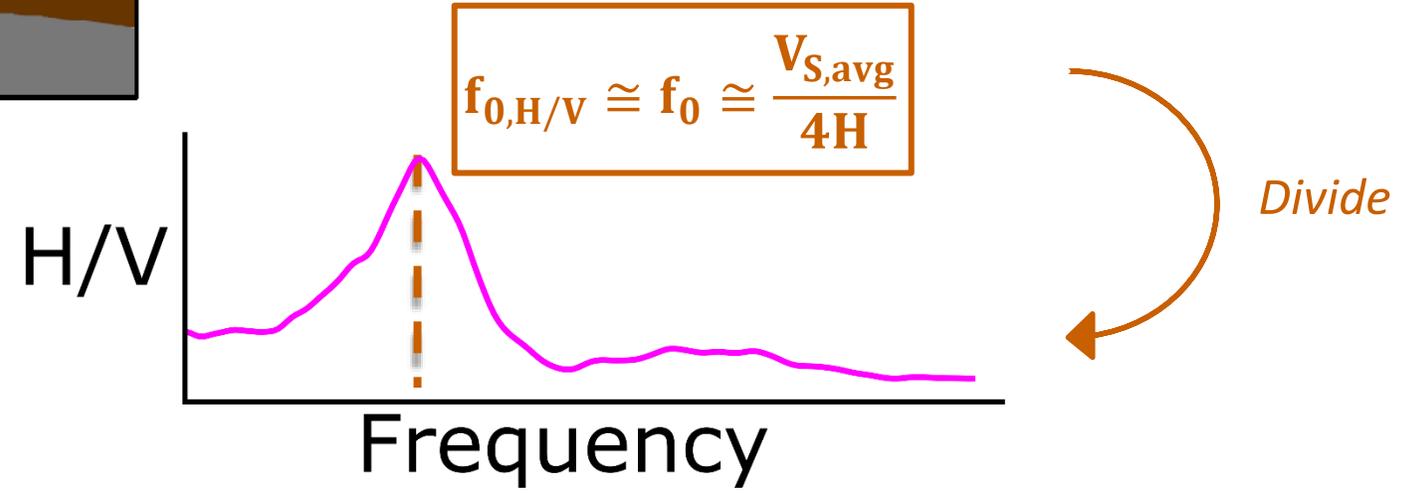
I wouldn't do a site response project without HVSR measurements!

Horizontal-to-Vertical Spectral Ratio (HVSR or H/V)

Nogoshi and Igarashi (1971), Nakamura (1989)



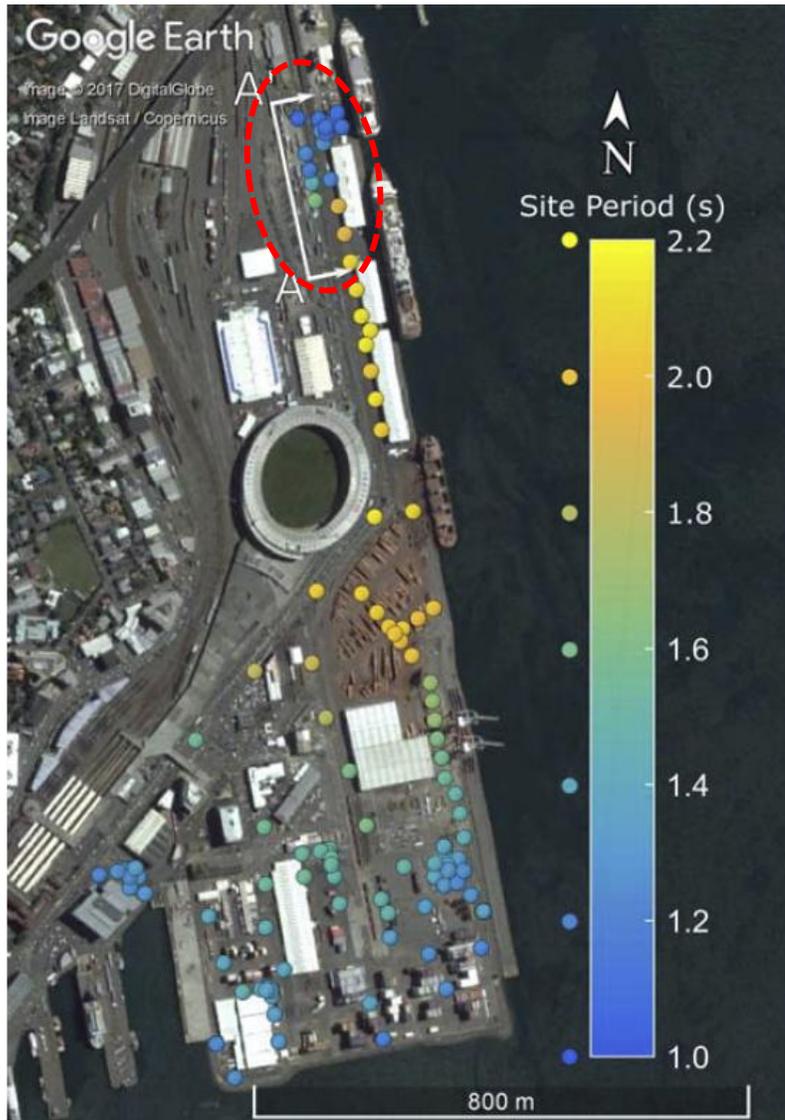
If an H/V curve exhibits a well-defined peak, the frequency corresponding to lowest-frequency peak ($f_{0,H/V}$) can be used to estimate the fundamental shear wave resonant frequency of the site (f_0) [Lermo and Chávez-García 1993; Lachet and Bard 1994; SESAME 2004]



Using HVSR to Assess Spatial Variability

CentrePort, Wellington, New Zealand

Damaged by the Mw = 7.8 2016 Kaikoura EQ



Vantassel et al. (2018)



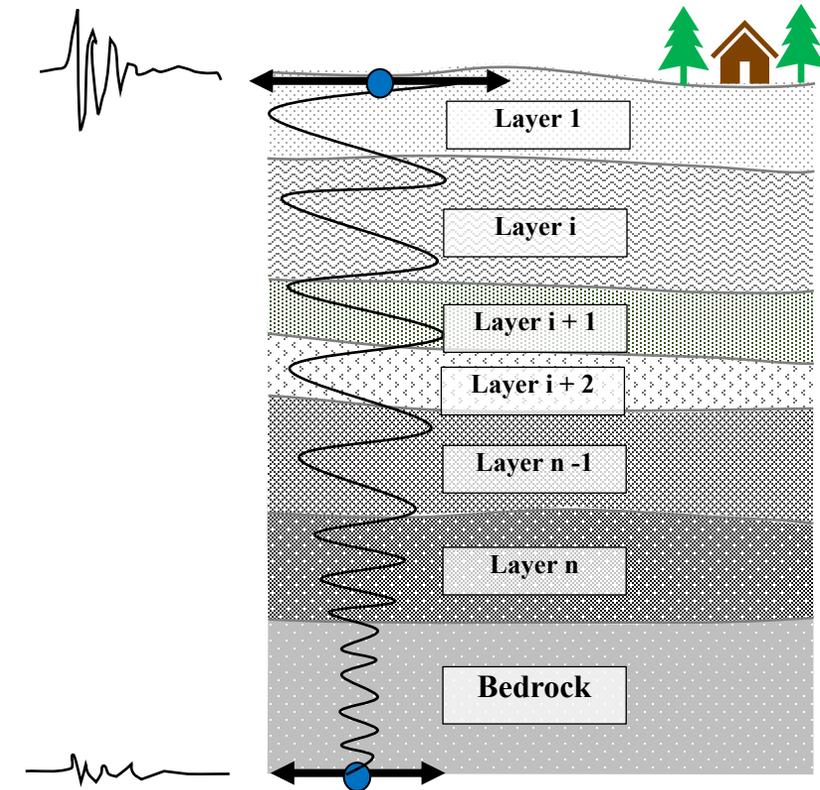
- 114 H/Vs measurement locations
- Significant spatial variability in $f_0 = (1/T_0)$
- Azimuthal variability in f_0
- 1D site response is not appropriate

Back to Site Effects

Seismic Ground Response Analysis (GRA)

Ground Model:

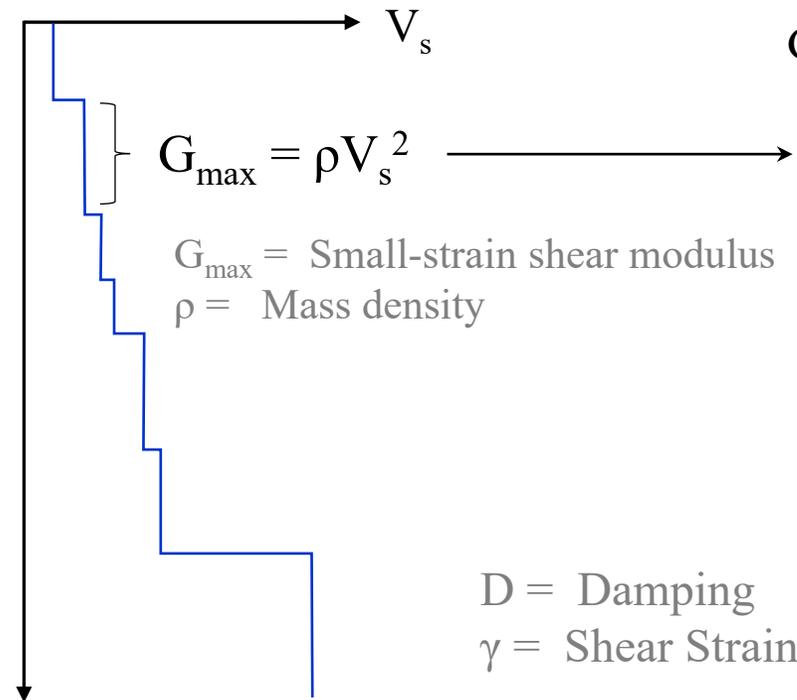
Output/Surface Motion



Input/Rock Motion

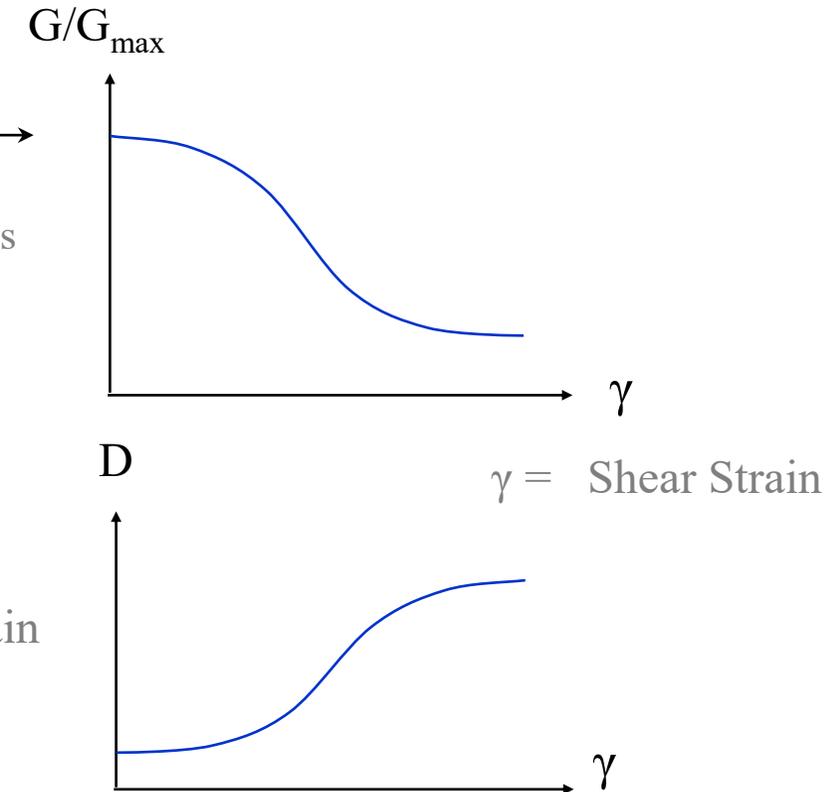
Field Measurements

In-Situ
Shear Wave Velocity (V_s)

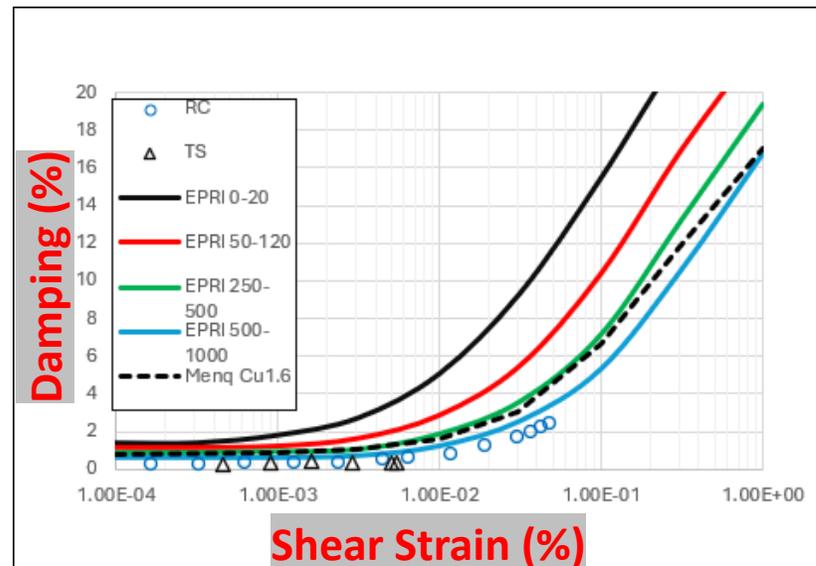
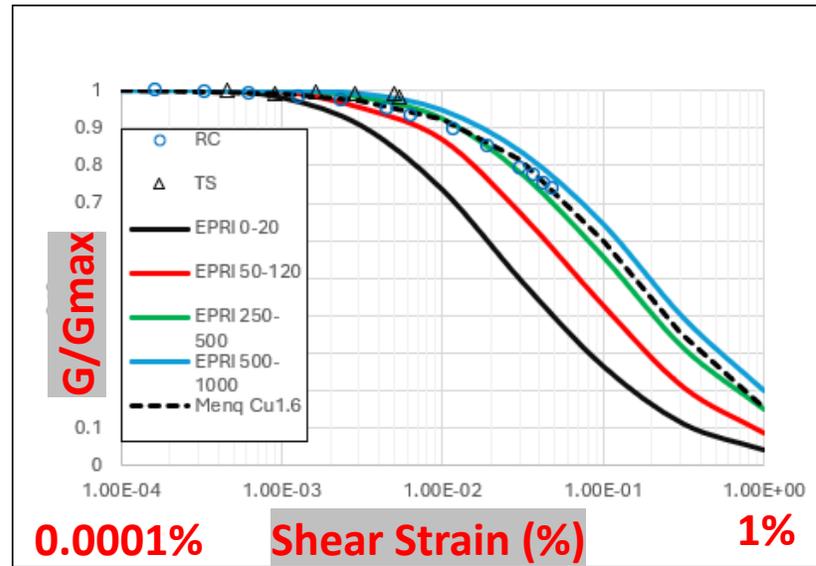


Lab Measurements

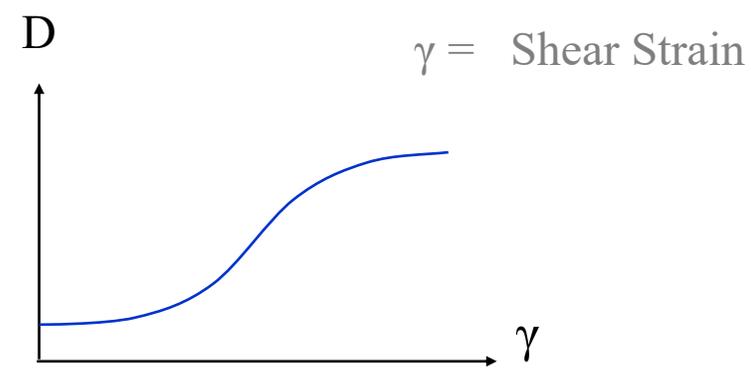
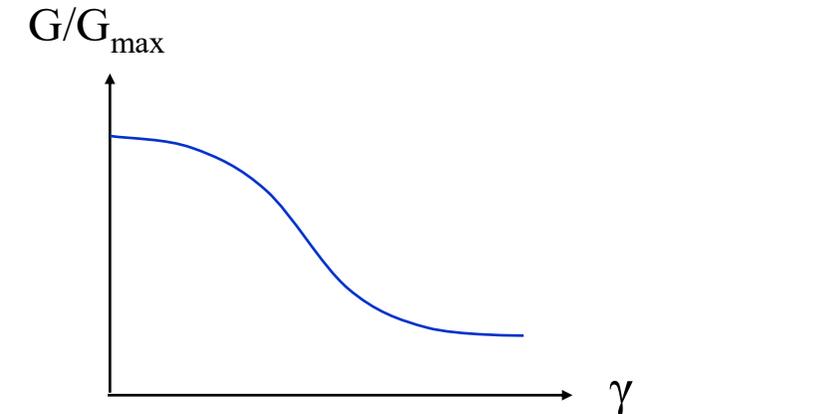
Nonlinear Shear Modulus (G) and Damping (D)



Seismic Ground Response Analysis (GRA)

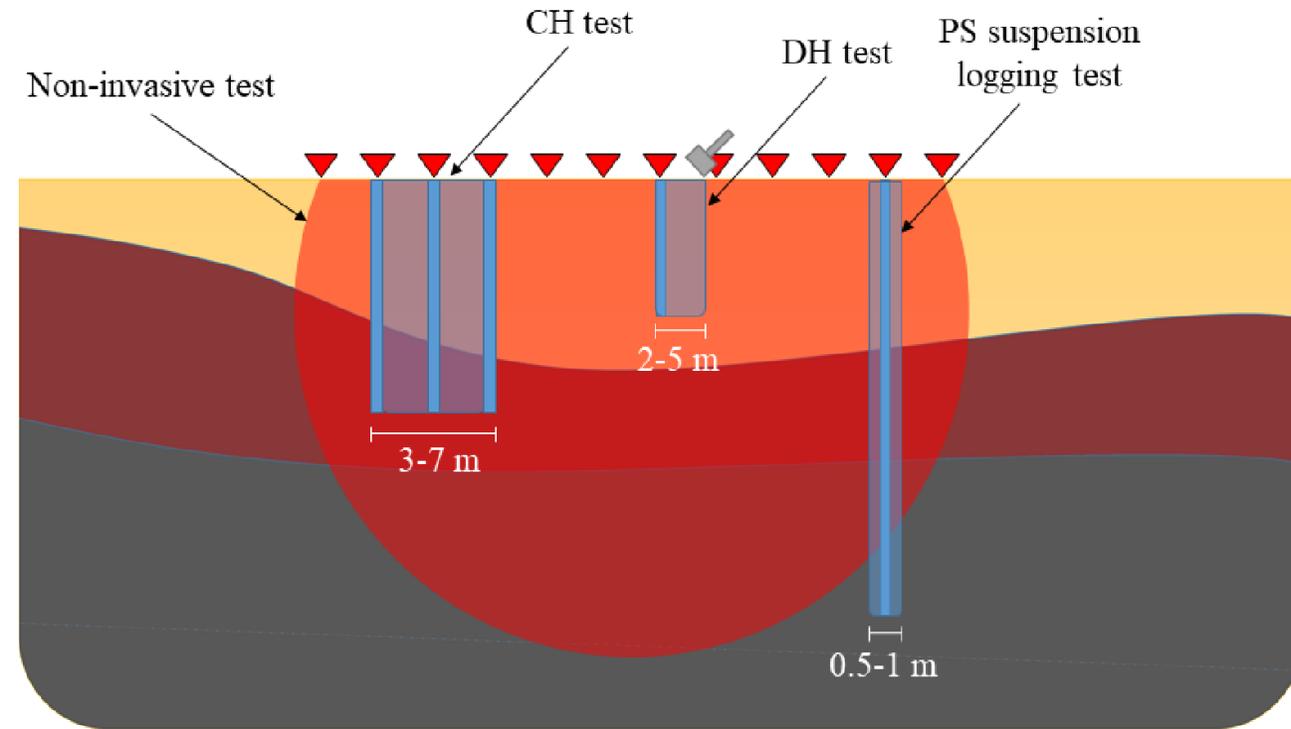


Lab Measurements
Nonlinear Shear Modulus (G) and Damping (D)



Field Measurements of Vs

- Invasive vs. Non-Invasive Seismic Wave Measurements



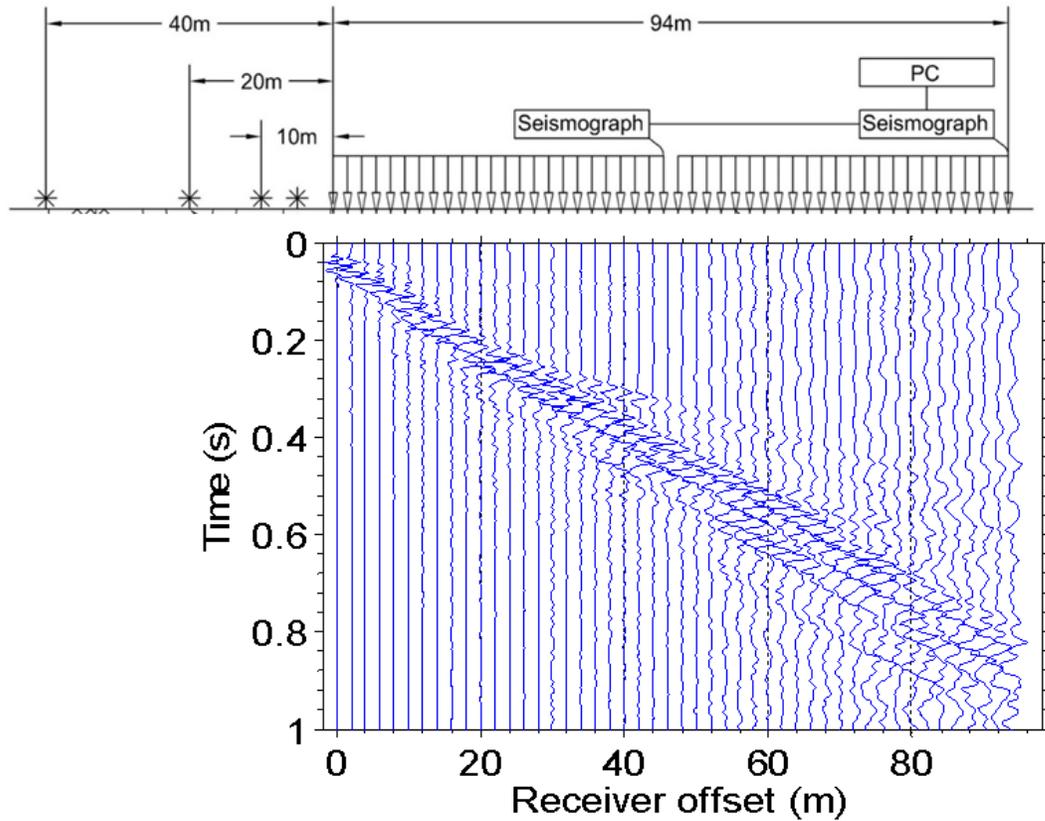
	Invasive Tests	Non-Invasive Tests
Pro	<ul style="list-style-type: none"> Direct measurements: simple and accurate interpretation Good resolution of thin layers Easier standardization Additional information from borehole logging or cone penetration 	<ul style="list-style-type: none"> Costs and flexibility (in time and space) Average properties (dynamic behaviour of the entire soil deposit) Large volumes are investigated
Cons	<ul style="list-style-type: none"> Costs and necessity of planning well in advance Local measurement 	<ul style="list-style-type: none"> Complex interpretation (indirect measurements based on inversion procedures or heavy processing) Layer resolution decreases with depth
Depth	<ul style="list-style-type: none"> DH & CH generally limited to top 60 m PS logging > 1 km 	<ul style="list-style-type: none"> Refraction generally limited to top 30 m – 50 m Surface waves 1m to > 1 km

Surface Wave Methods

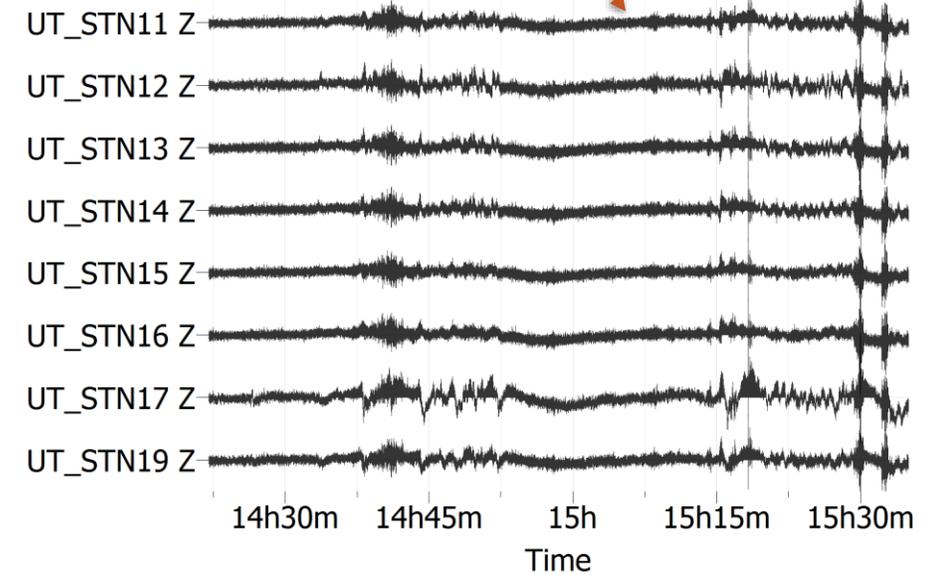
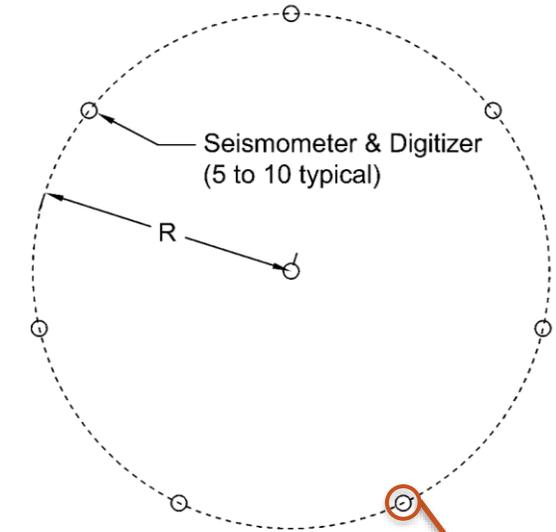
- Many different methods with various acquisition, processing, and inversion techniques. Can generally be grouped as follows:
- Active-source:
 - SASW: spectral analysis of surface waves (Stokoe et. al 1994)
 - MASW: multi-channel analysis of surface waves (Park et al. 1999, Foti 2000)
- Passive-source:
 - ReMi™: refraction microtremor with *linear arrays* (Louie 2001)
 - MAM: microtremor array measurements with *2D arrays* (Okada 2003, Tokimatsu et al. 1992)

MASW and MAM Overview

MASW



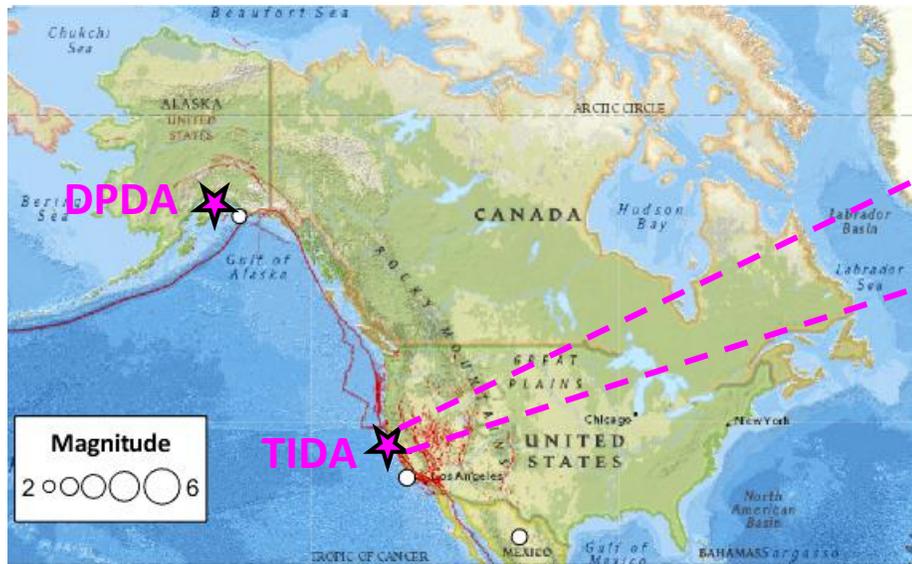
MAM



Application at Downhole Array Sites

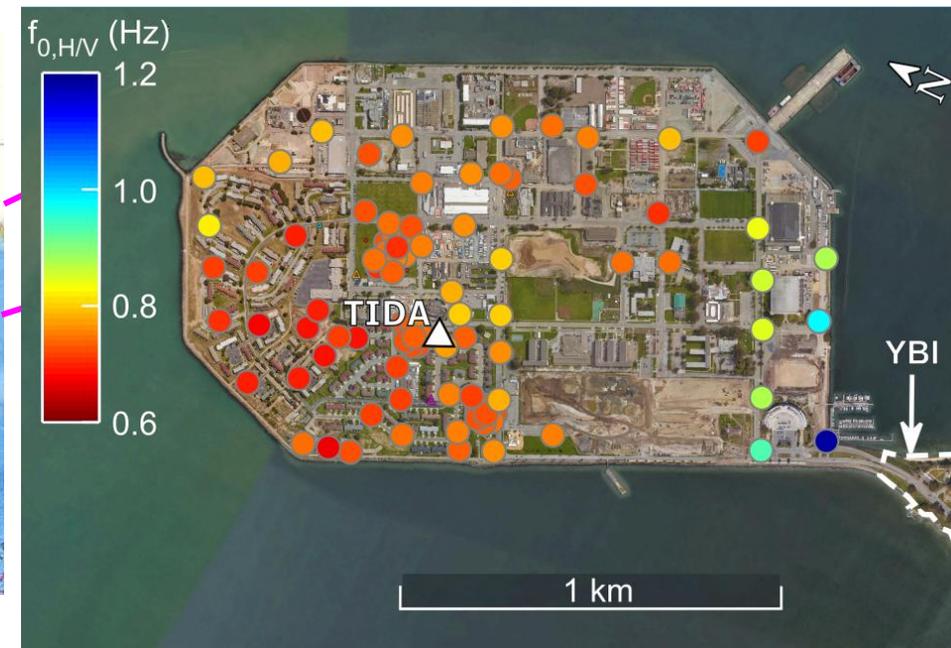
- Treasure Island Downhole Array (TIDA)
- Delaney Park Downhole Array (DPDA)

Earthquakes over the past 30 days



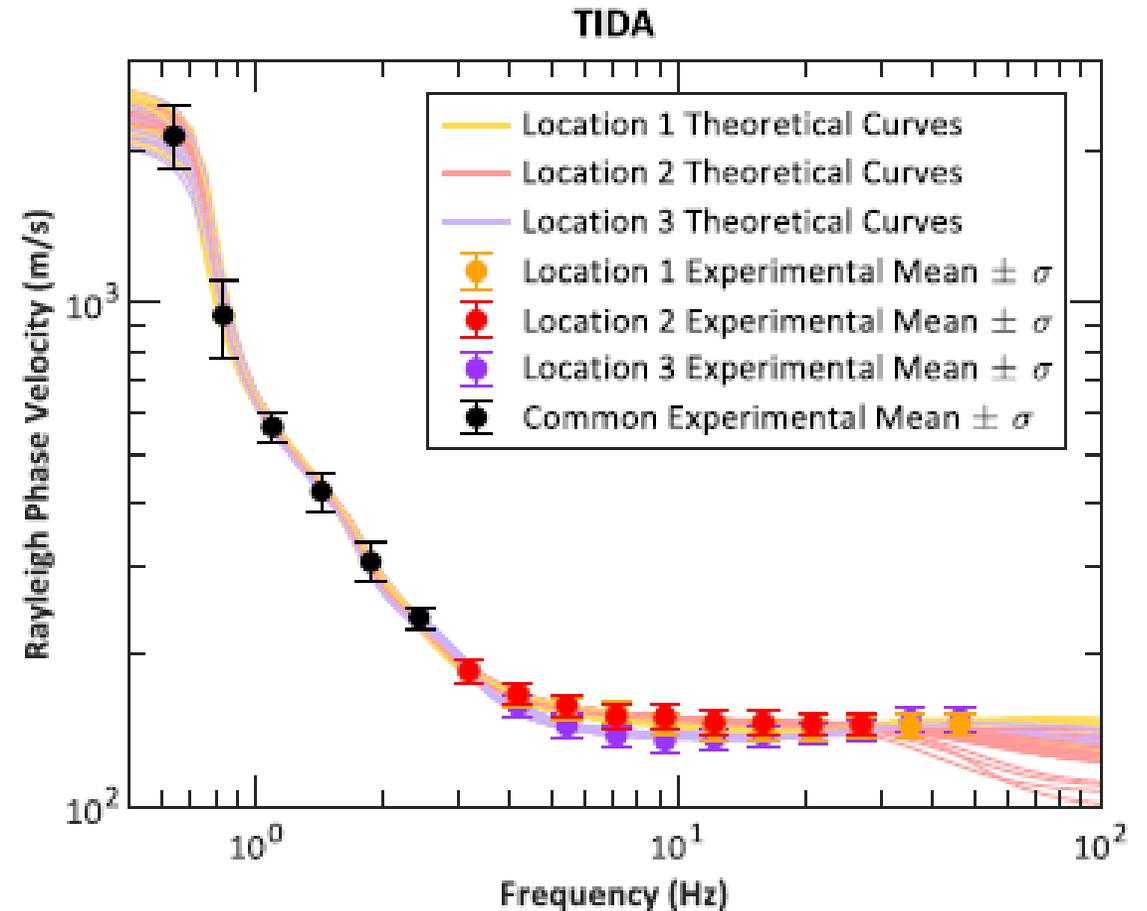
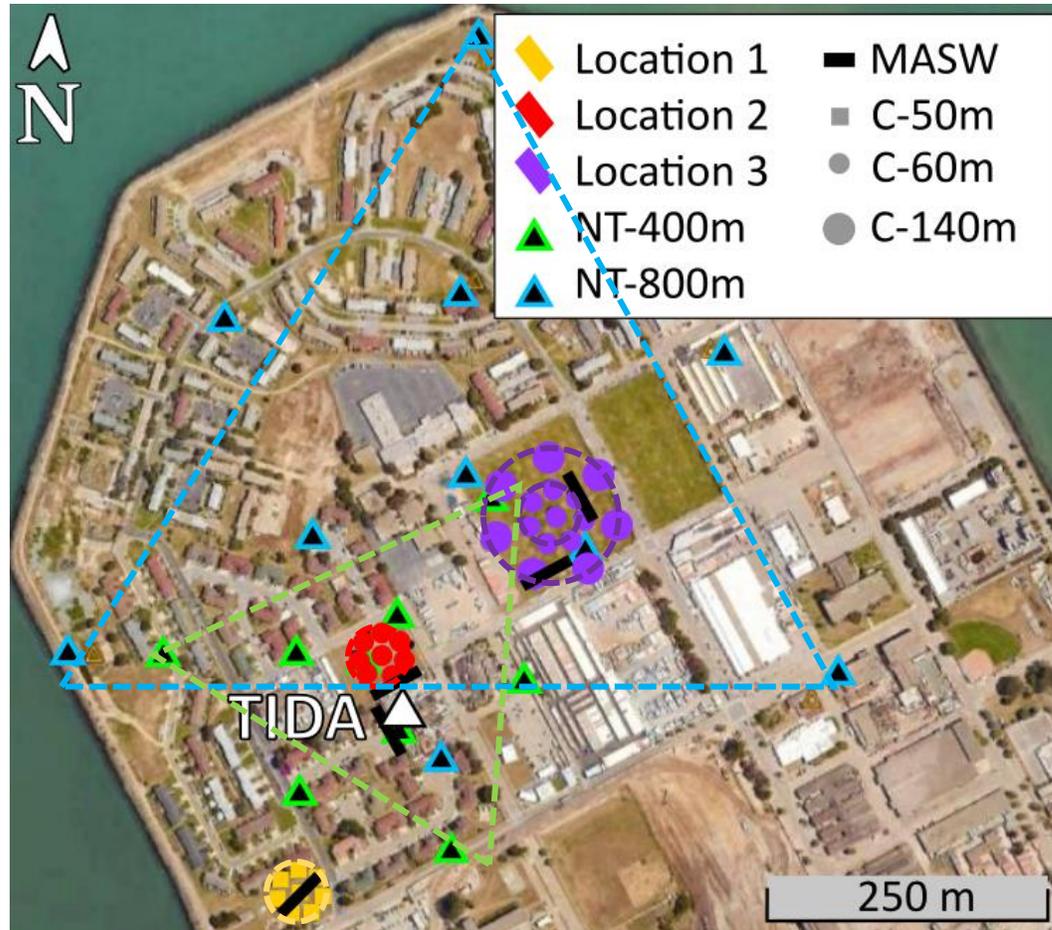
Source: USGS (accessed 03/10/2021)

~100 H/V Measurements



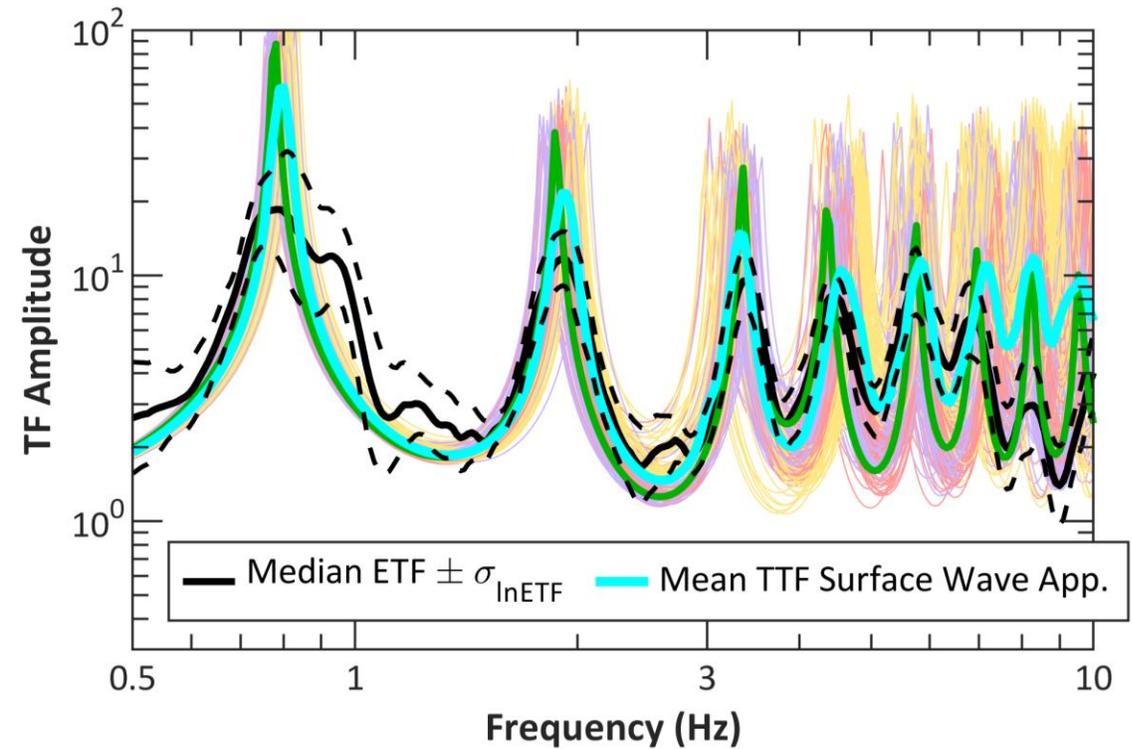
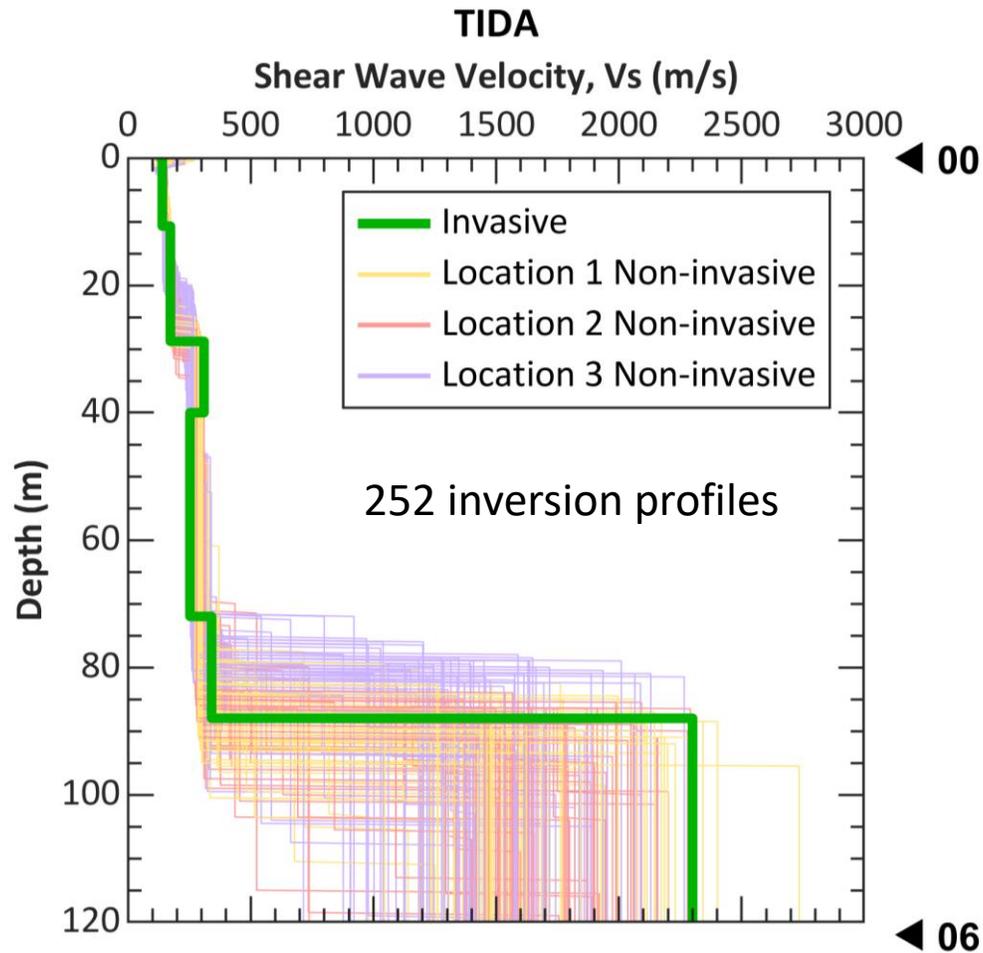
Example - Surface Wave Testing at TIDA

- Testing at 3 distinct locations to explicitly consider spatial variability using MASW and MAM arrays



Hallal et al. (2022)

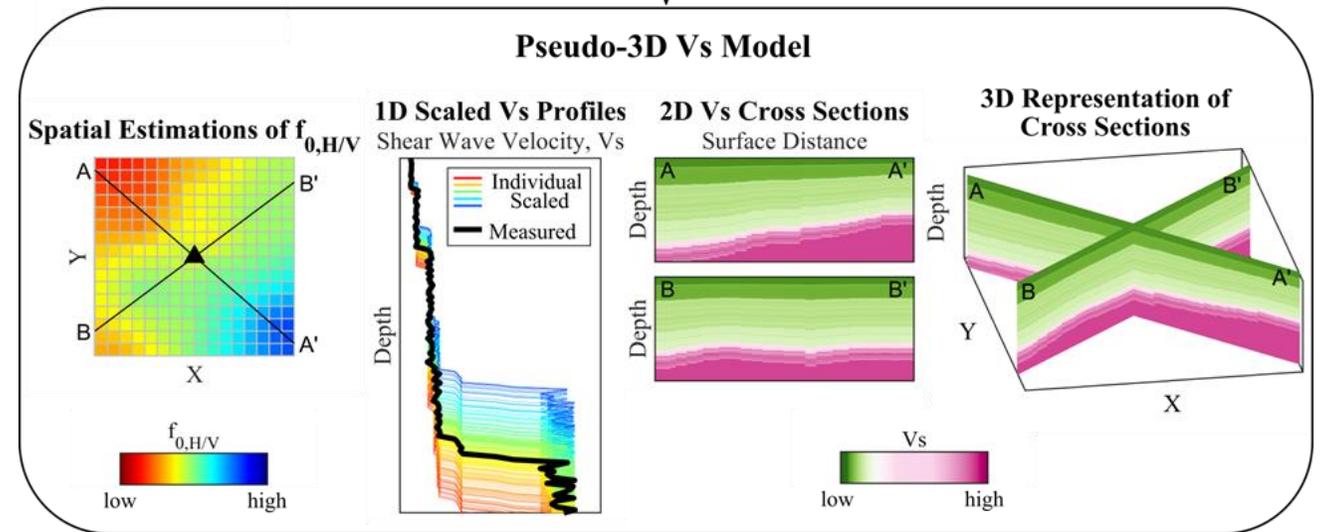
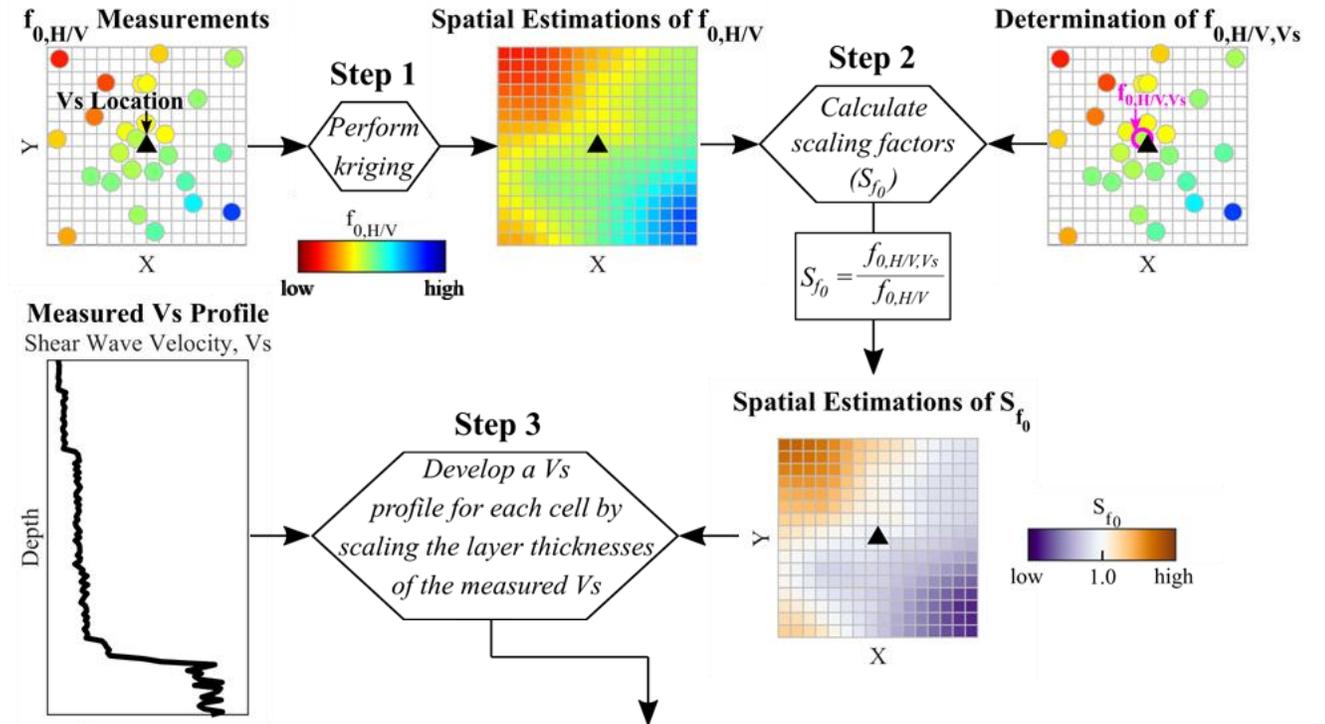
Example - Surface Wave Testing at TIDA



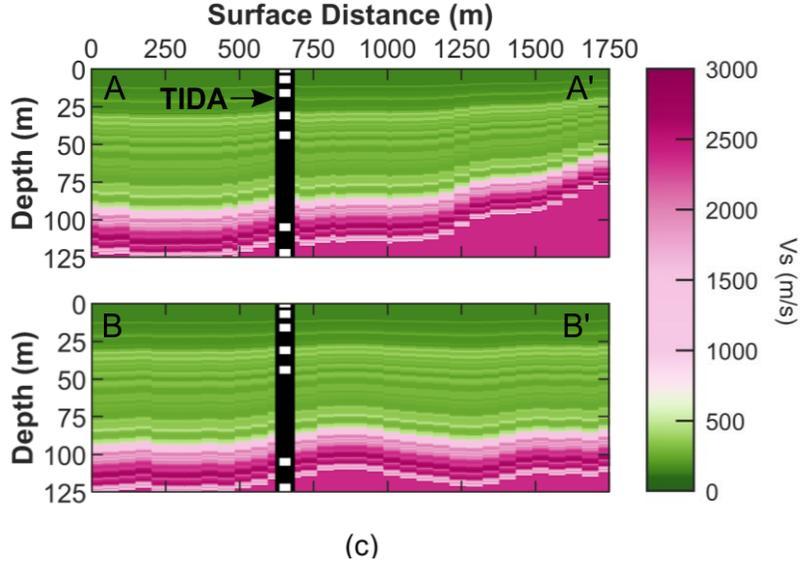
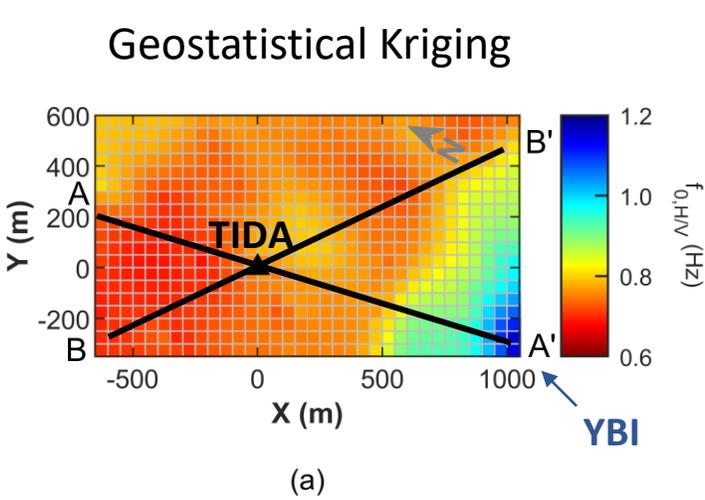
Hallal et al. (2022)

H/V Geostatistical Approach for Building Pseudo-3D Vs Models

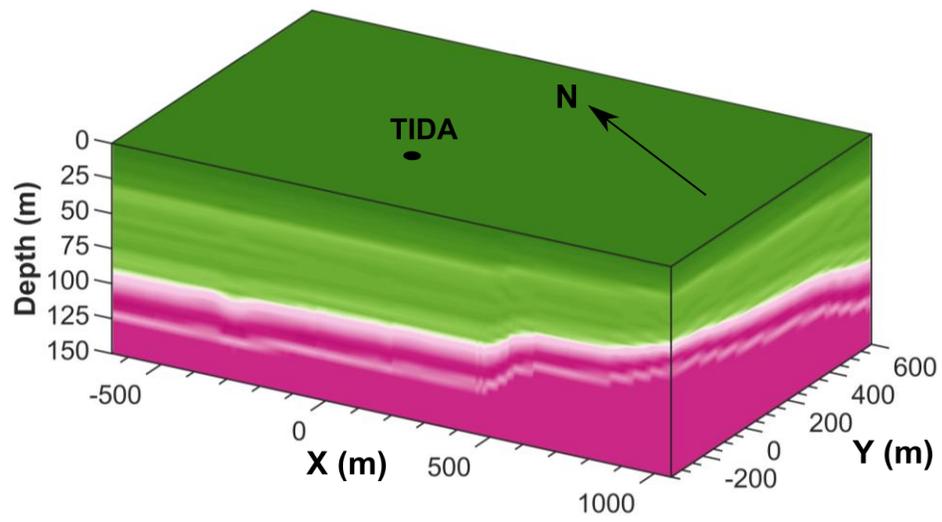
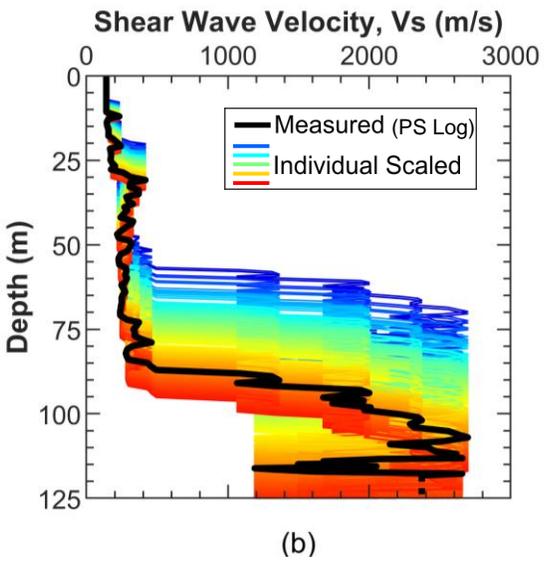
1. Hallal, M.M., Cox, B.R. (2021). "An H/V Geostatistical Approach for Building Pseudo-3D Vs Models to Account for Spatial Variability in Ground Response Analyses I: Model Development," *Earthquake Spectra*, (<https://doi.org/10.1177/8755293020981989>).
2. Hallal, M.M., Cox, B.R. (2021). "An H/V Geostatistical Approach for Building Pseudo-3D Vs Models to Account for Spatial Variability in Ground Response Analyses II: Application to 1D Analyses at Two Downhole Array Sites," *Earthquake Spectra*, (<https://doi.org/10.1177/8755293020981982>).



Pseudo-3D Vs Model at TIDA from H/V Geostatistical Approach



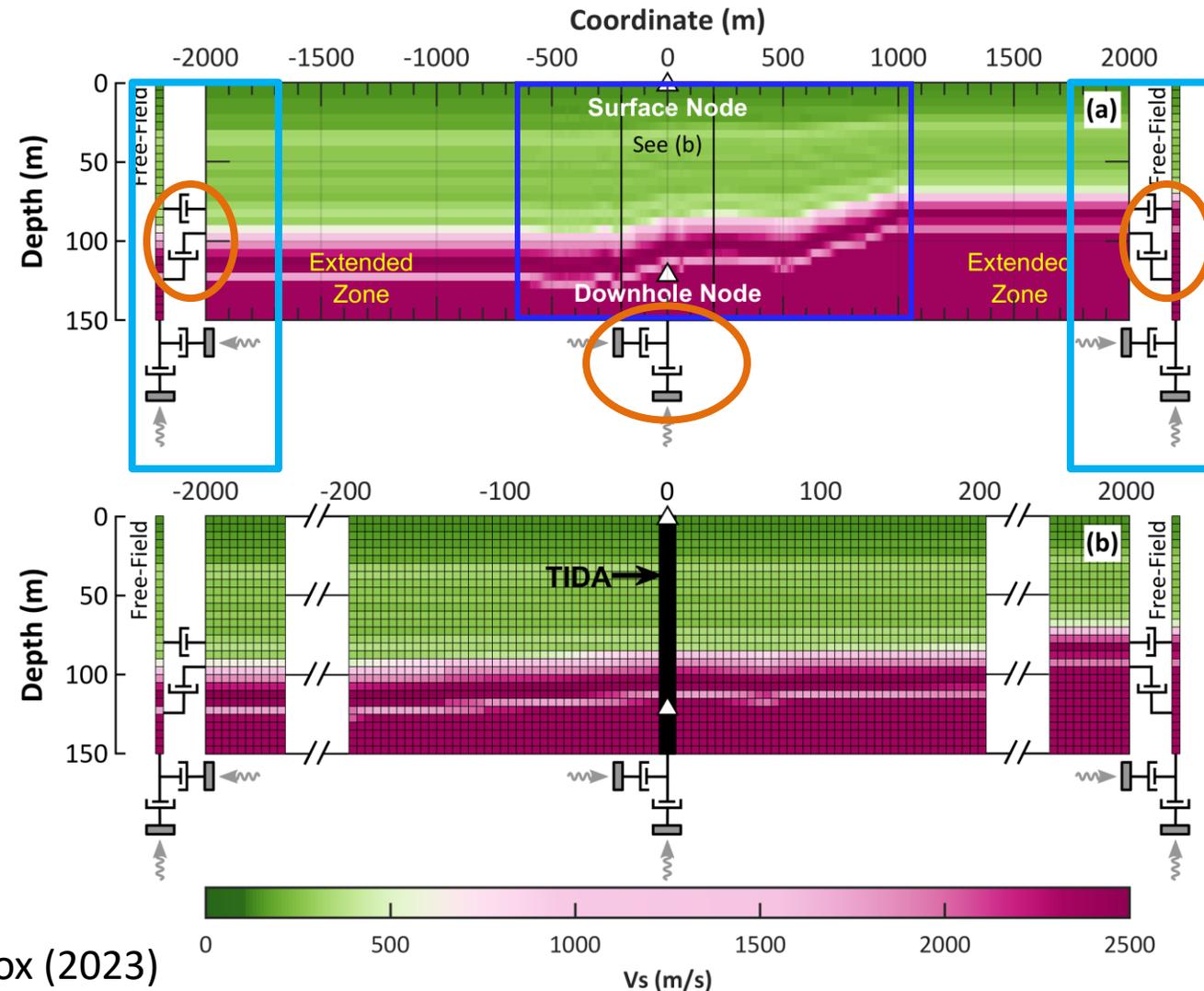
Scaled Vs Profiles



2D GRAs at TIDA: Model Details

- 5-m quadrilateral elements
- 4,000 m × 150 m (extended to minimize boundary effects)
- 24,000 elements
- Free-field boundary conditions
 - Shear- and compression-wave dashpots at side and base boundaries
 - 1D equivalent free-field input at side boundaries
- Run time: 13 mins for single core execution on TACC (Stampede2)

Numerical Model



Hallal & Cox (2023)

Comparing Simulations (TTFs) to Observations (ETFs)

How large of an area influences seismic site response?

- Observation:

- ETF

- Predictions:

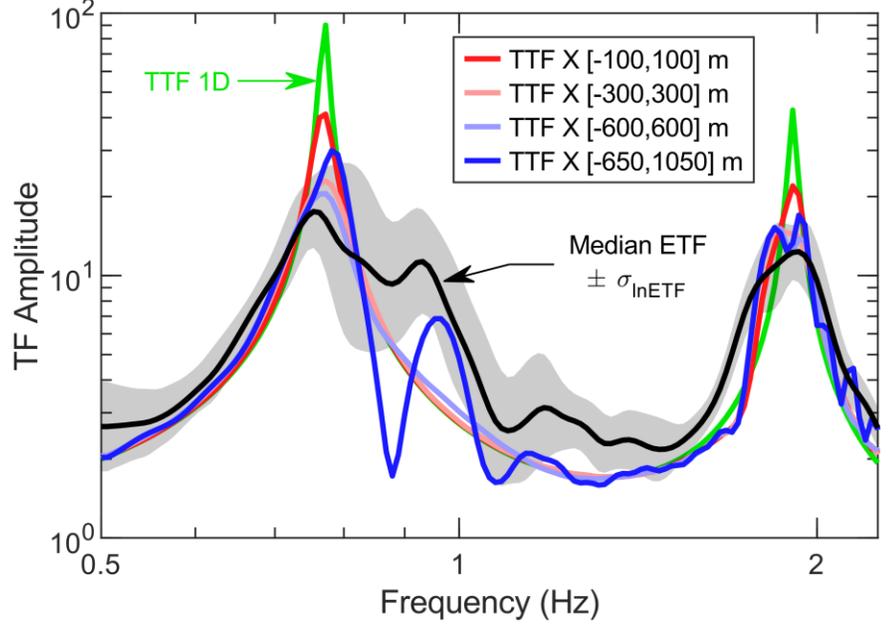
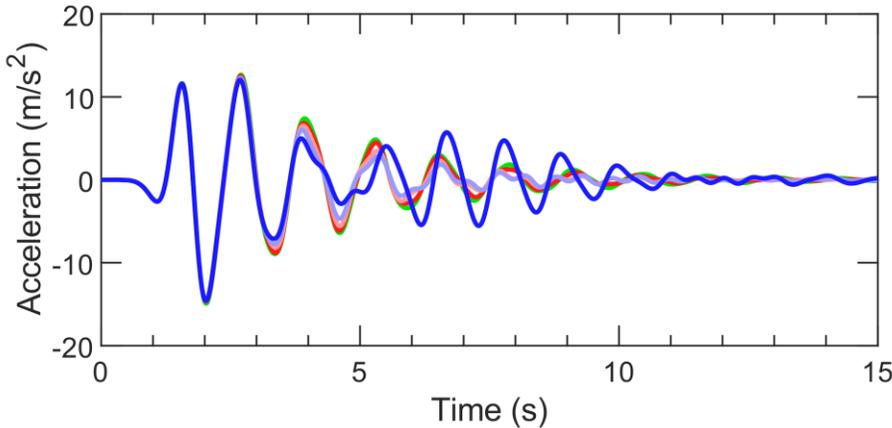
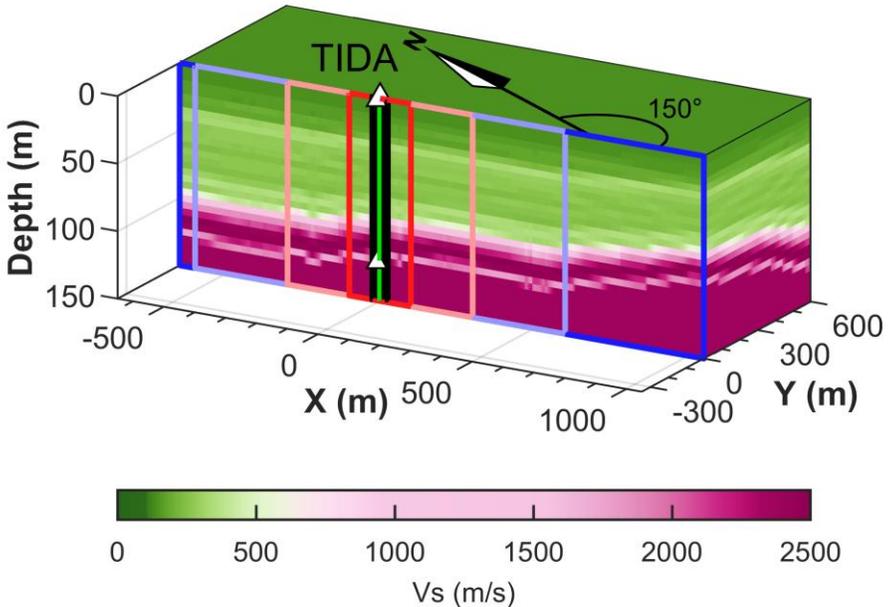
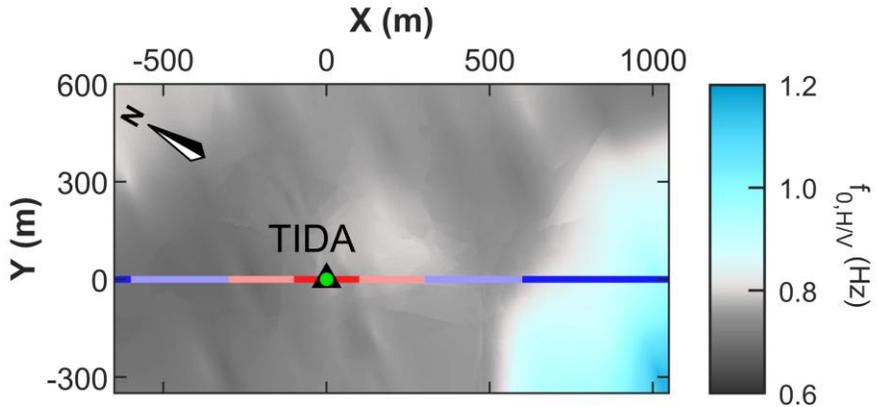
- 1D (i.e., ~0 m)

- [-100, 100] m

- [-300, 300] m

- [-600, 600] m

- [-650, 1050] m



Hallal & Cox (2023)

Hornsby Bend DAS Dataset

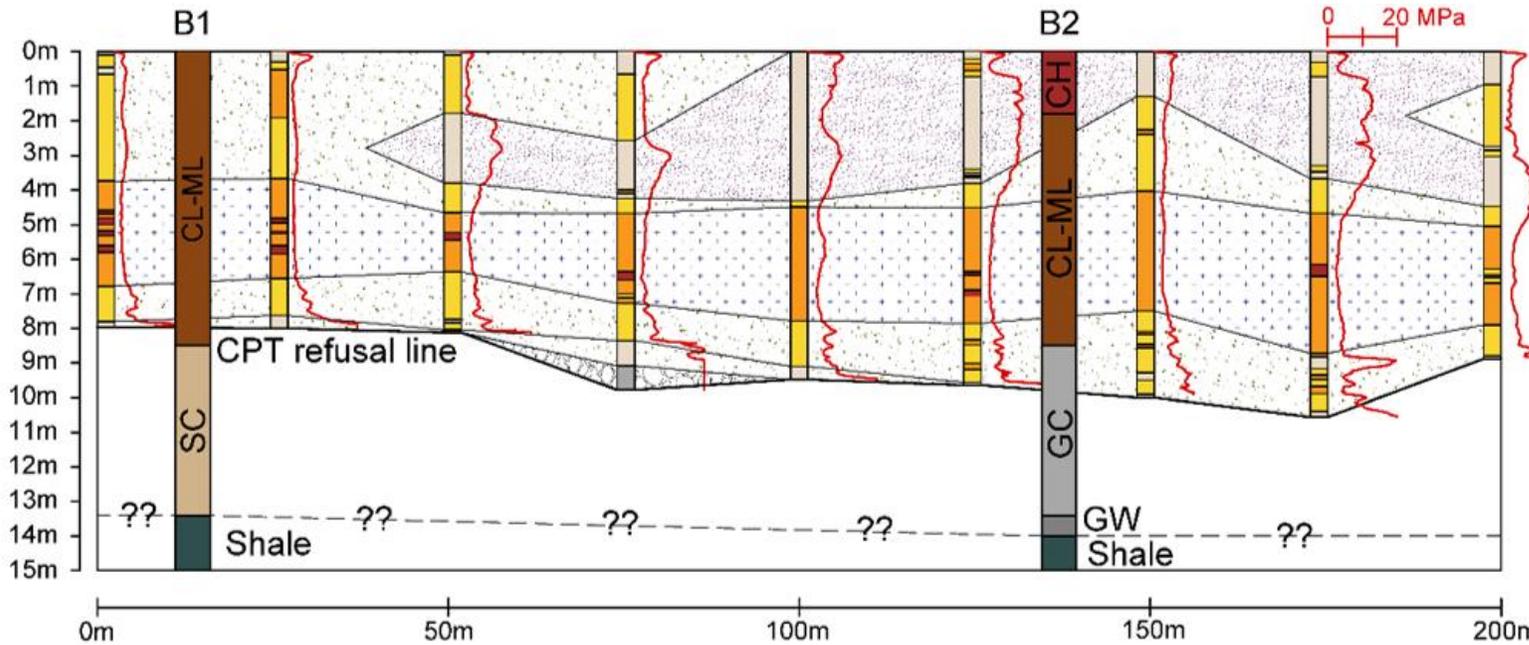
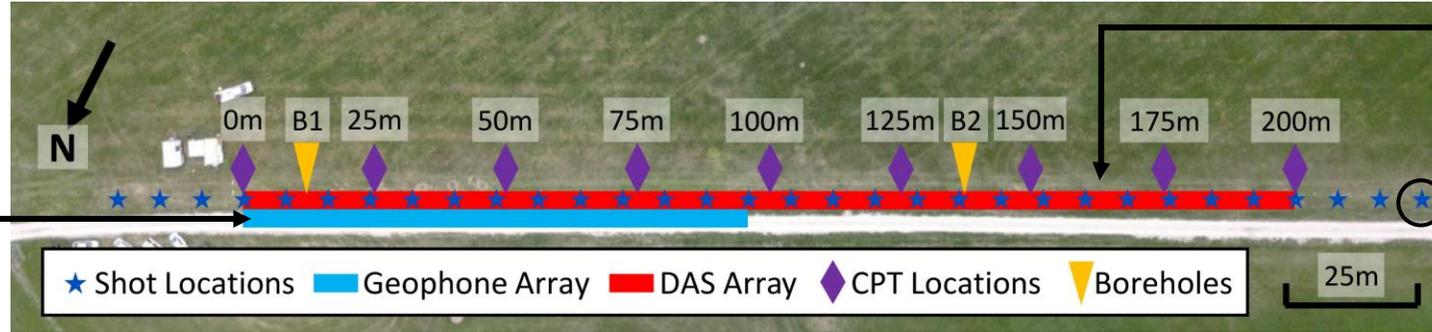
SITE DESCRIPTION AND TESTING SETUP



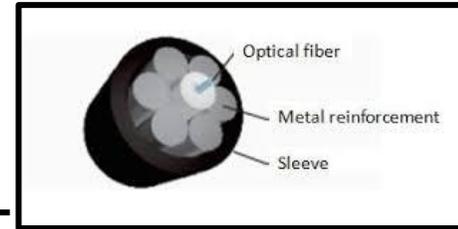
GeoSpace
GS-11D 4.5-Hz
Geophones
48 Vert. at 2m spacing,
48 Horz. at 2m spacing



Geometrics Geode
24-ch. Seismographs
(four)



Clay Silt Mix Sand Mix Sand Gravel q_c



NanZee Sensing
Technology (NZS-
DSS-C02) fiber-optic
cable



OptaSense ODH4+
2m GL,
1m channel spacing



NHERI@UTexas
Thumper Truck

Hornsby Bend DAS Dataset – Journal Paper 1



sensors

Hubbard et al. (2022)

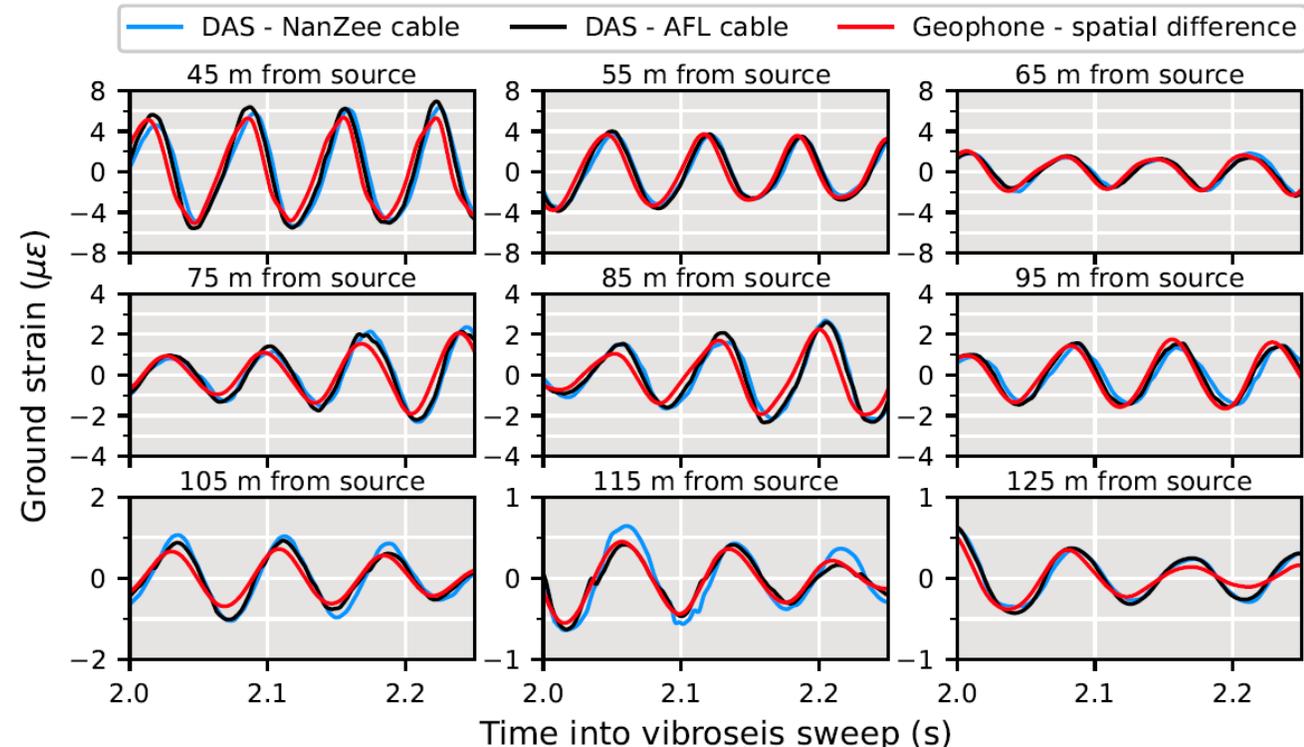
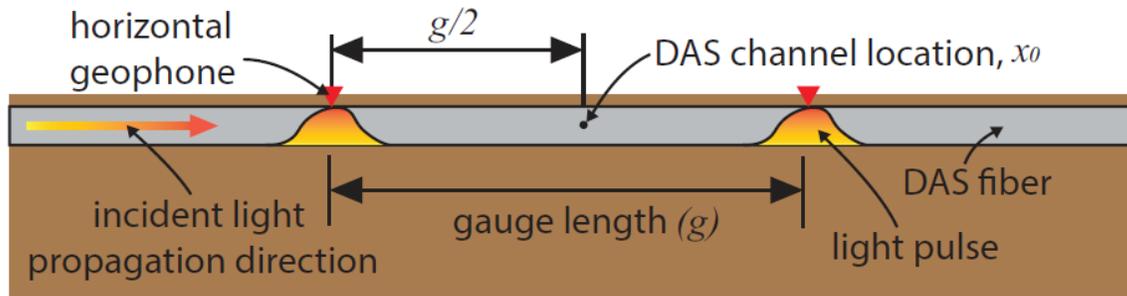


Article

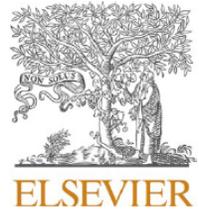
Quantifying the Surface Strain Field Induced by Active Sources with Distributed Acoustic Sensing: Theory and Practice

Peter G. Hubbard ^{1,*}, Joseph P. Vantassel ², Brady R. Cox ³, James W. Rector ¹, Michael B. S. Yust ² and Kenichi Soga ¹

Nearly identical signals are obtained from DAS and horizontal geophones oriented in-line with the fiber optic cable



Hornsby Bend DAS Dataset – Journal Paper 2



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Journal of Applied Geophysics

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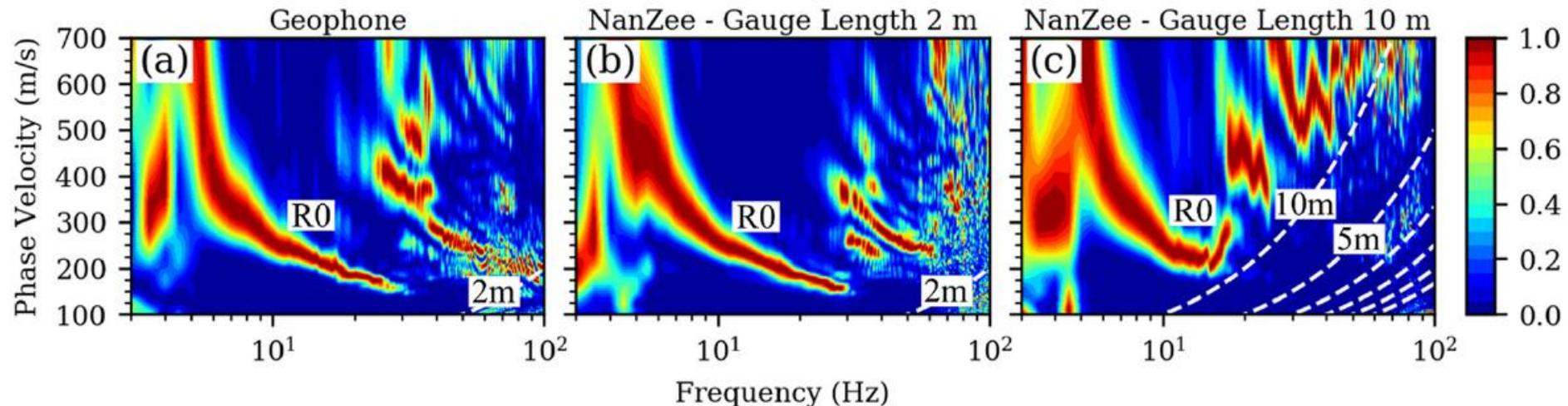
Vantassel et al. (2022)



Resolution of dispersion data at high frequencies is governed by the smaller of either the gauge length (GL) or 2-times the channel separation (in order to satisfy spatial aliasing criteria).

Extracting high-resolution, multi-mode surface wave dispersion data from distributed acoustic sensing measurements using the multichannel analysis of surface waves

Joseph P. Vantassel^{a,*}, Brady R. Cox^b, Peter G. Hubbard^c, Michael Yust^a



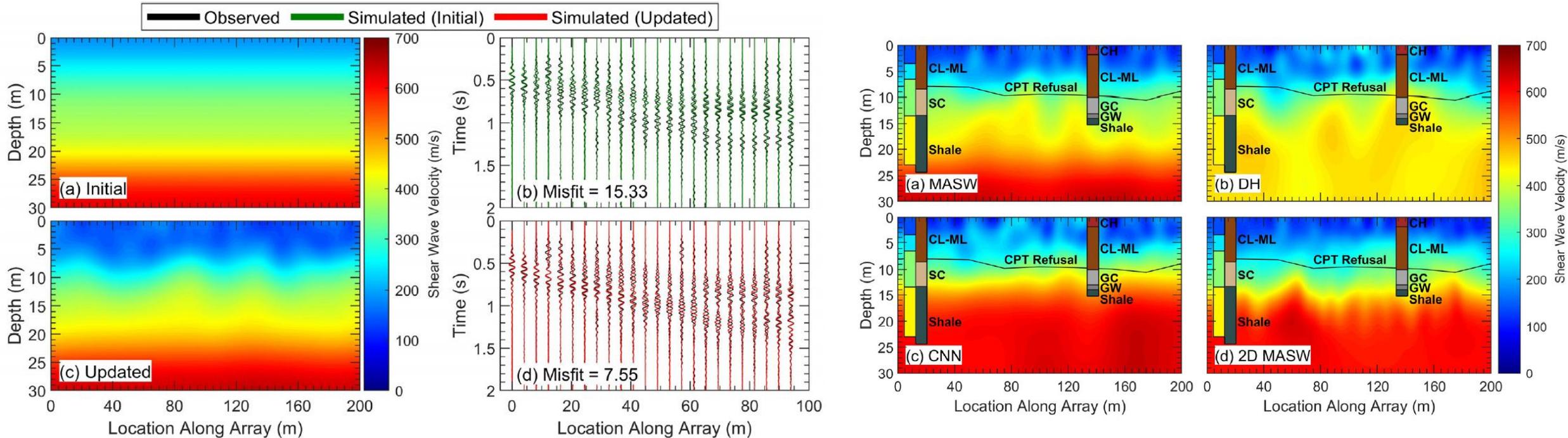
Hornsby Bend DAS Dataset – Journal Paper 3

Article

Near-Surface 2D Imaging via FWI of DAS Data: An Examination on the Impacts of FWI Starting Model

One of the first journal articles on full waveform inversion (FWI) of DAS data.

Michael B. S. Yust^{1,*} , Brady R. Cox^{2,*}, Joseph P. Vantassel³ , Peter G. Hubbard⁴, Christian Boehm⁵ and Lion Krischer⁵

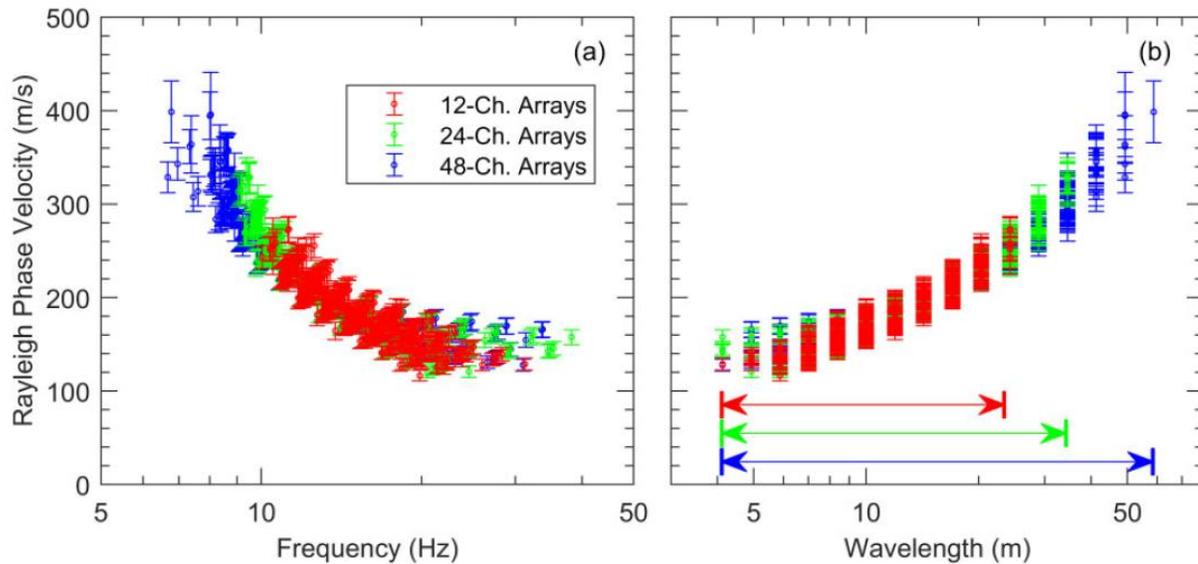


Hornsby Bend DAS Dataset – Journal Paper 4

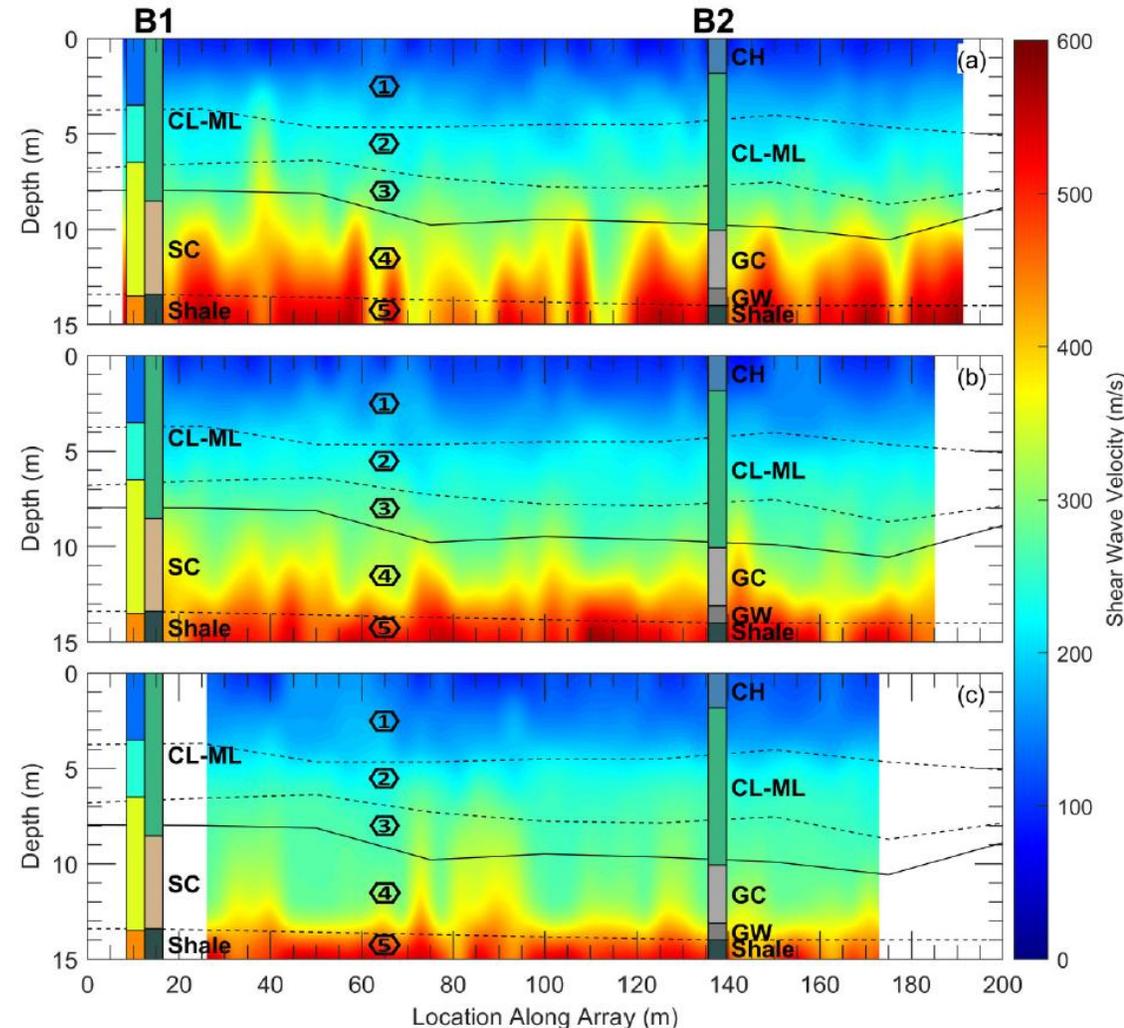
Yust et al. (2024)

DAS for 2-D MASW imaging: a case study on the benefits of flexible subarray processing

Michael B. S. Yust¹, Brady R. Cox², Joseph P. Vantassel³ and Peter G. Hubbard⁴

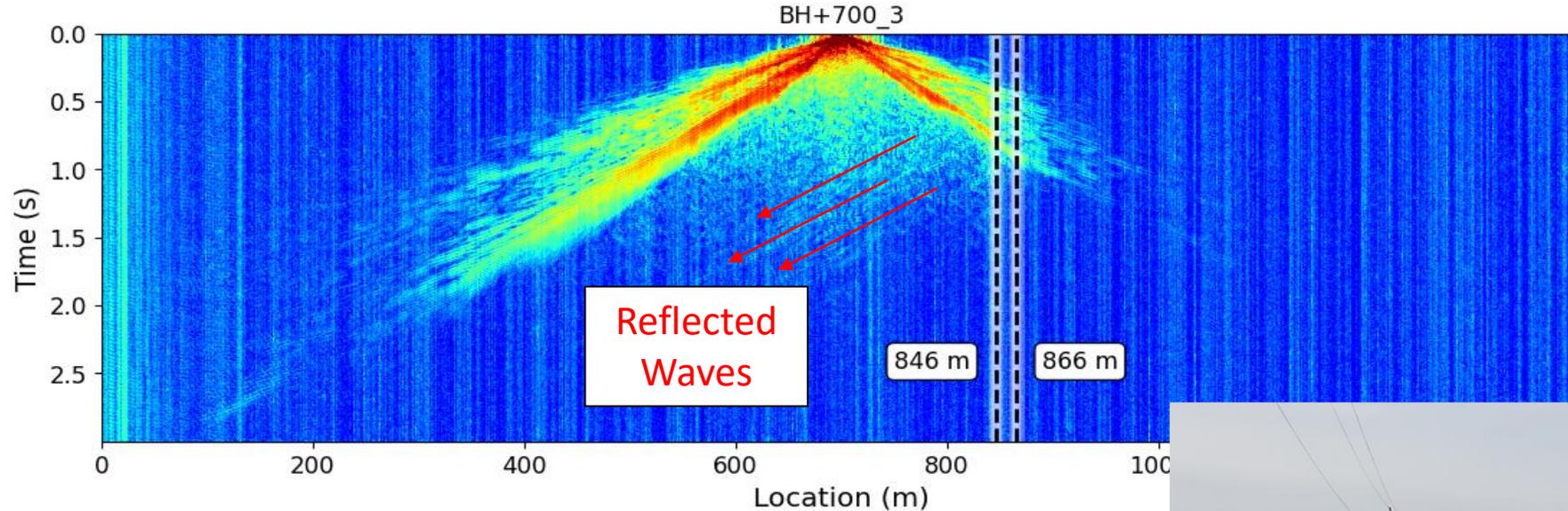


DAS is extremely beneficial for 2D subsurface imaging using methods like FWI and/or pseudo-2D MASW



Two Recent, Un-published DAS Studies

- Imaging the Southern San Andreas Fault (SSAF)



- Monitoring strain induced by a transmission tower implosion along a levee in the Sacramento Delta



The Earthquake Critical Zone (ECZ)

- NSF FRES Project

“Collaborative Research: Bridging geoscience and engineering to interrogate seismic cycle processes in the earthquake critical zone”

PI: A. Ault; Co-PI's: S. Akciz, B. Cox, G. Hirth, D. Newell, S. Shreedharan



**Distributed Acoustic Sensing:
Data Acquisition and Initial Data Processing**

**Southern San Andreas Fault (SSAF)
Painted Canyon, Mecca Hills, CA**

Painted Canyon

Legend

— SSAF (USGS)



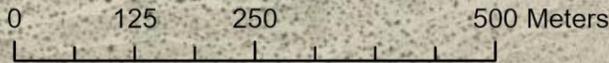
0 125 250 500 Meters

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Painted Canyon

Legend

- SSAF (USGS)
- As-Built DAS Array ~ 1.5 km



0m

835m

1500m

Esri Community Maps Contributors, County of Riverside, California State Parks, © OpenStreetMap, Microsoft, Esri, TomTom, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, US Census Bureau, USDA, USFWS, Maxar

Installing the Fiber Optic Cable



- Tight-buffered cable

DAS Interrogator Settings



Conversion from Phase to Microstrain:

$$\hat{\epsilon} = \frac{\Lambda d\phi}{4\pi n \xi g}$$

$\hat{\epsilon}$ = average microstrain over a gauge length of optical fiber

Λ = optical wavelength of the laser used in the DAS system [μm] ($\Lambda=1.55 \mu\text{m}$)

$d\phi$ = phase change [radians]

n = group refractive index of the sensing fiber ($n=1.4677$)

ξ = photoelastic scaling factor for longitudinal strain in an optical fiber ($\xi=0.78$)

g = gauge length [m] ($g=2.04 \text{ m}$)

Parameter	Value
Gauge length [m]	2.04
Spatial Sampling Interval [m/ch]	1.02
# of channels	1456
Pulse Rate [Hz]	40,000
Decimation Factor	4
Output Data Rate (unprocessed) [Hz]	10,000
Output Data Rate (processed) [Hz]	1,000
Fiber Refractive Index	1.4677
Laser Wavelength [nm]	1550
Photoelastic Scaling Factor	0.78
Raw Data Unit	$\frac{rad}{2\pi/2^{16}}$

Installing the SmartSolo 3C Nodal Stations

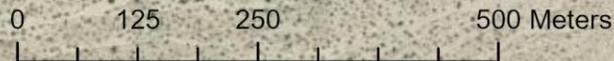


- 149 Stations
- Buried ~1m from the DAS line, every 10 m

SS Locations

Legend

- SS Stations
- SSAF (USGS)



0m

835m

1500m

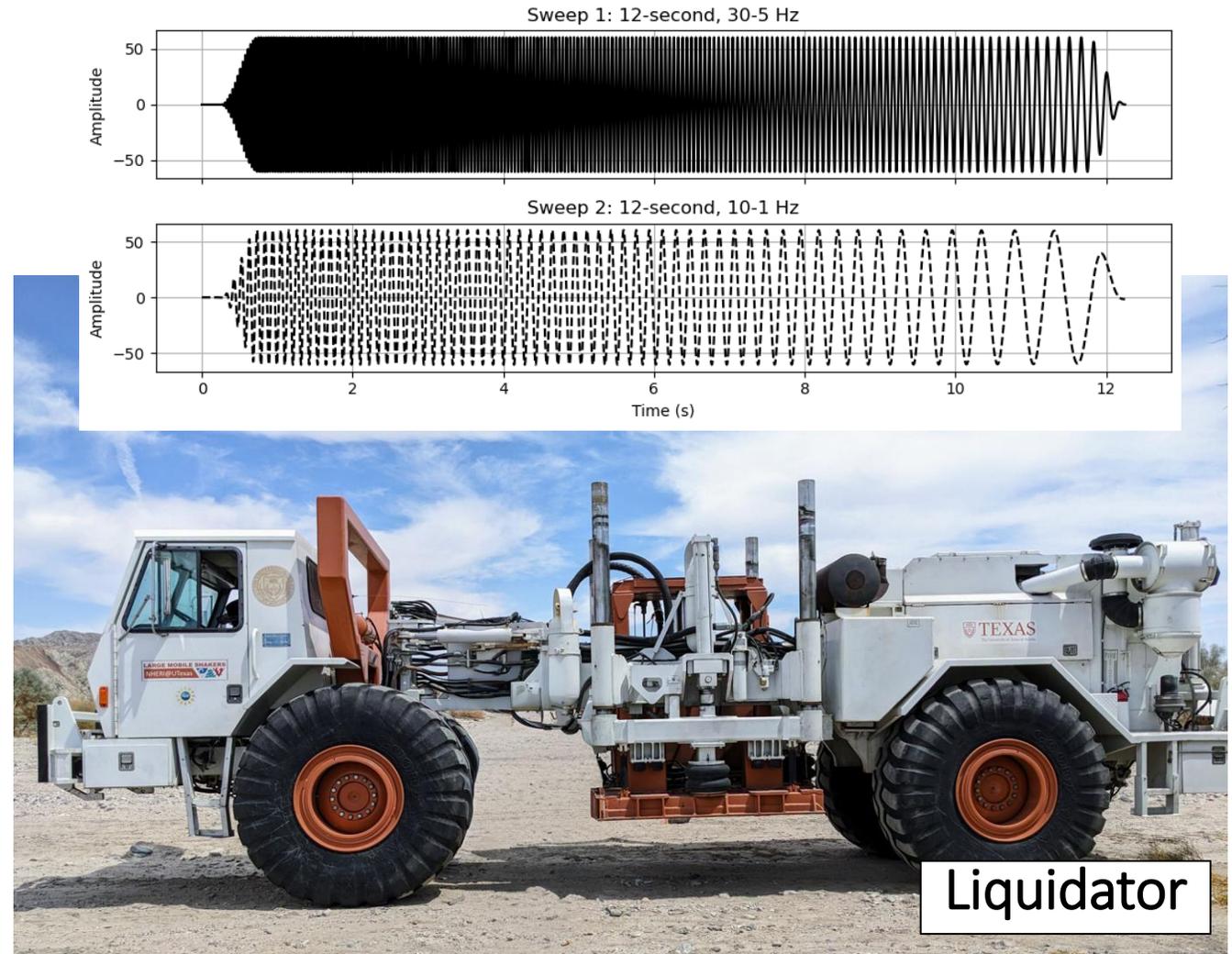
Painted Canyon Rd

Painted Canyon Rd

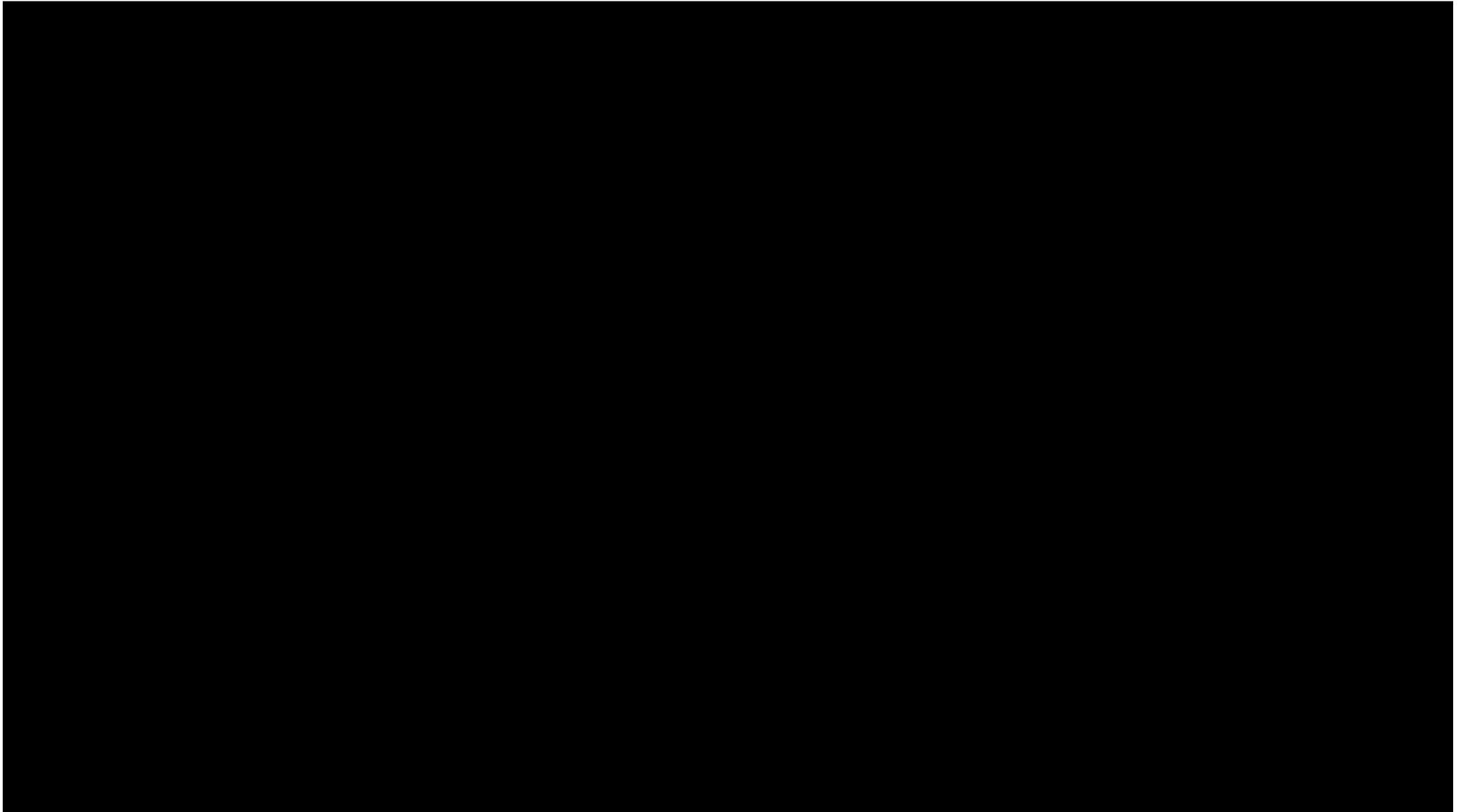
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Active-Source Testing

- Shot locations every 10m with a sledgehammer and Liquidator
- Liquidator Sweeps:



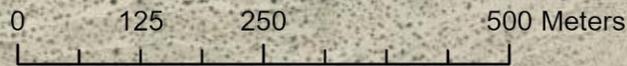
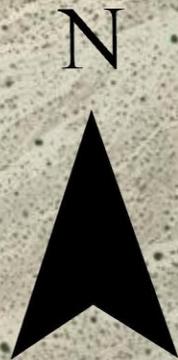
Liquidator Video



Active Testing Shot Locations

Legend

- Shot Locations
- SSAF (USGS)
- As-Built DAS Array



0m

700 m

835m

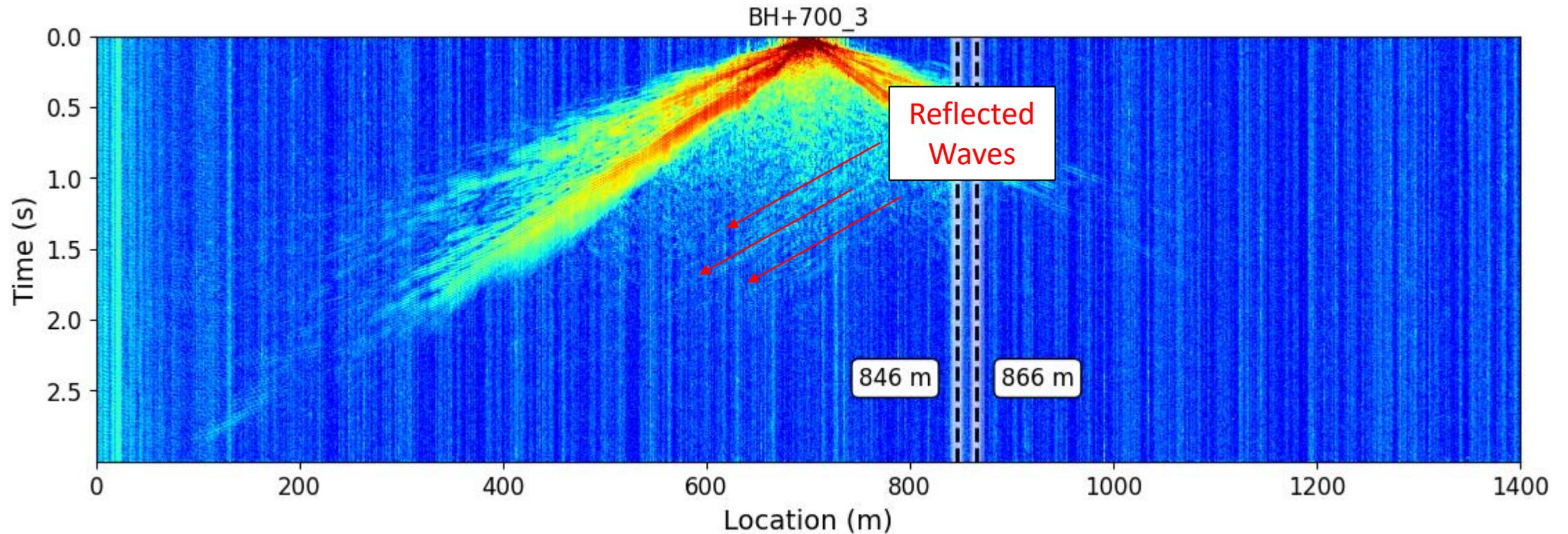
1500m

Painted Canyon Rd

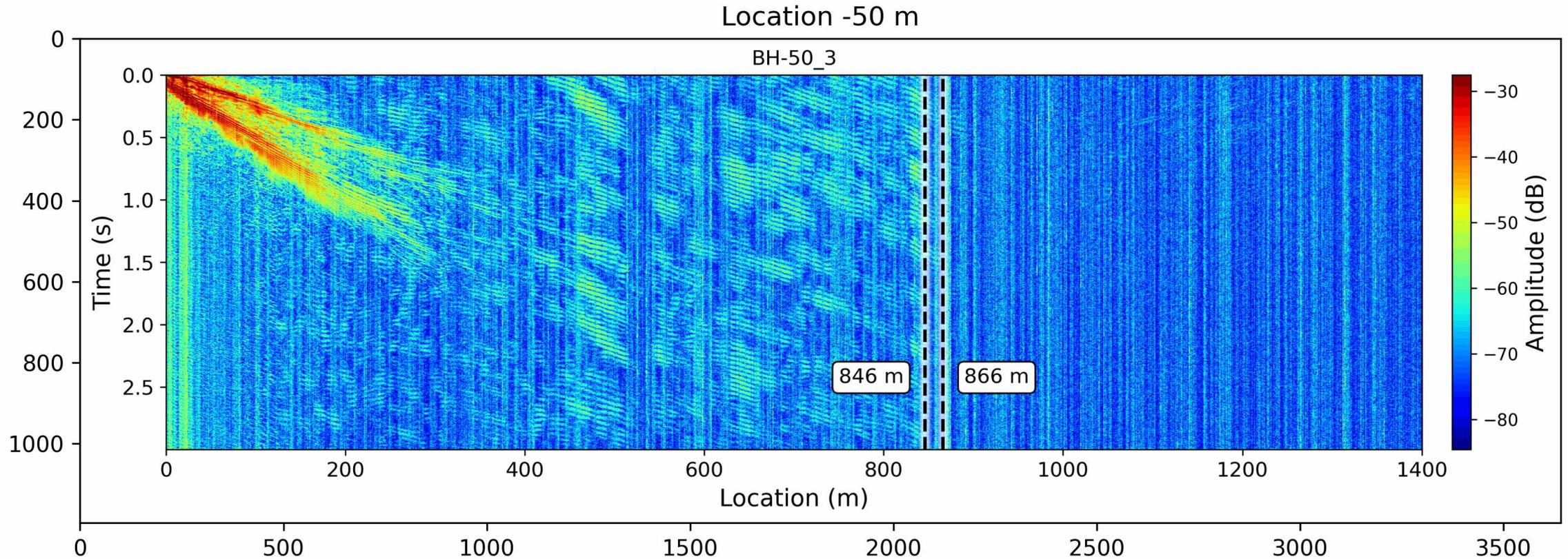
Painted Canyon Rd

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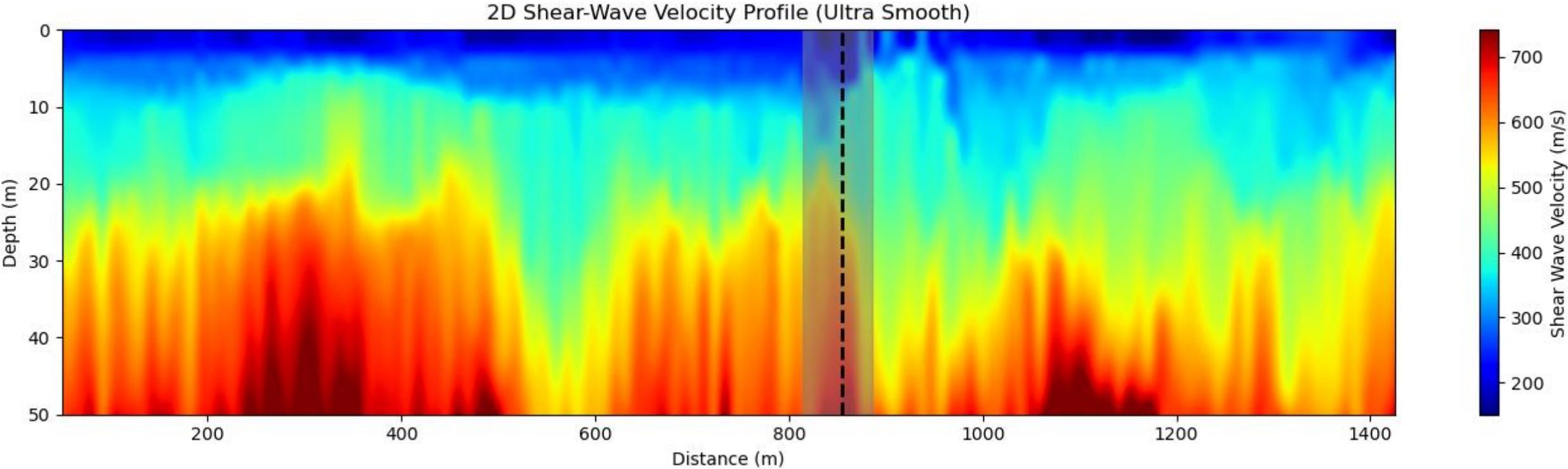
Sledgehammer Shot at 700 m



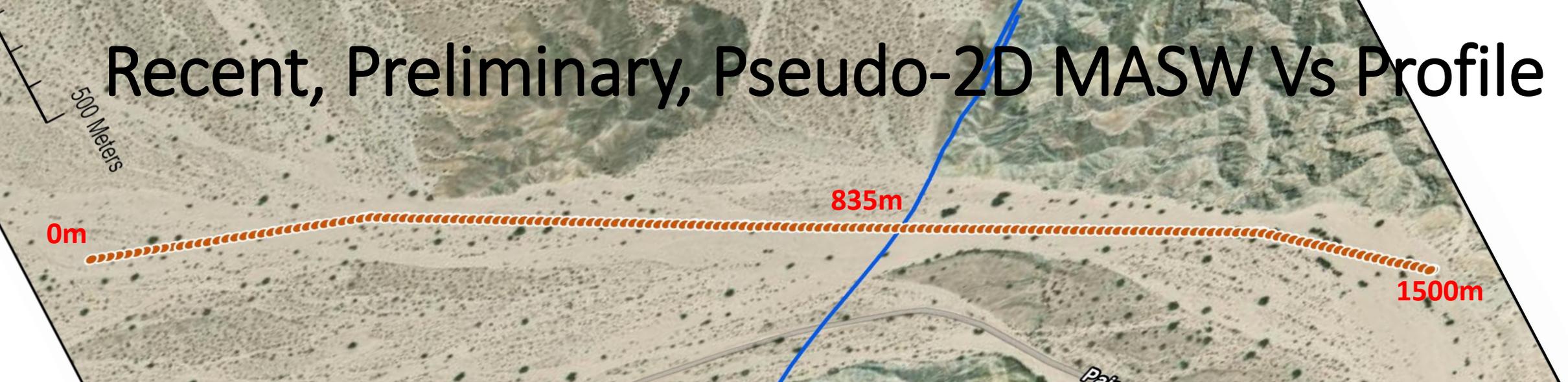
Animation of all Sledgehammer Shots



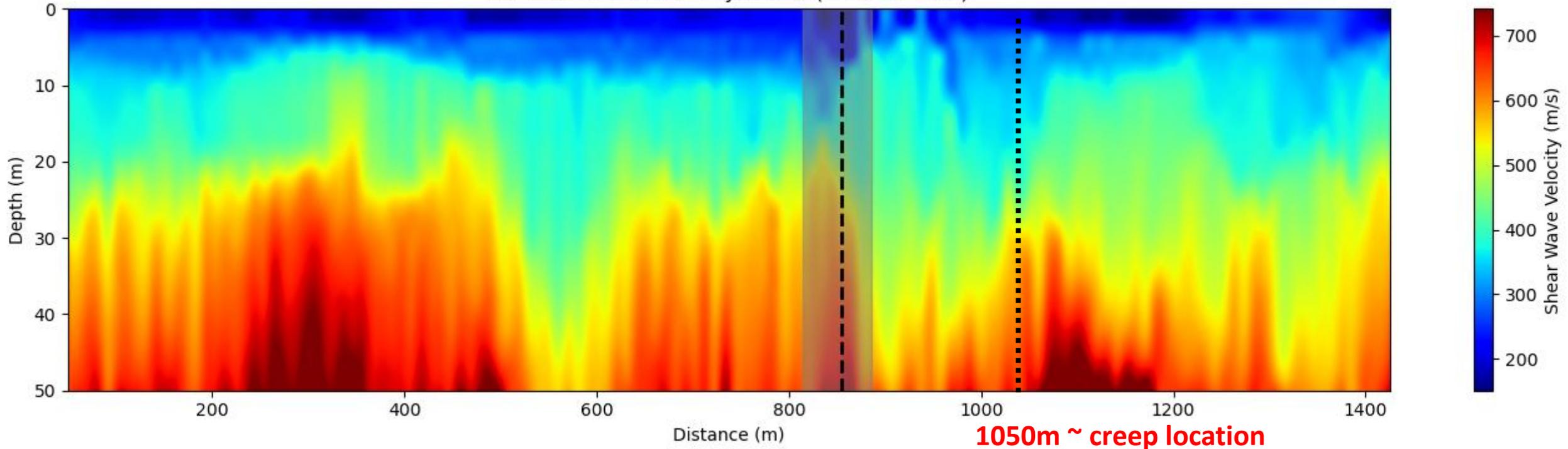
Recent, Preliminary, Pseudo-2D MASW Vs Profile



Recent, Preliminary, Pseudo-2D MASW Vs Profile



2D Shear-Wave Velocity Profile (Ultra Smooth)

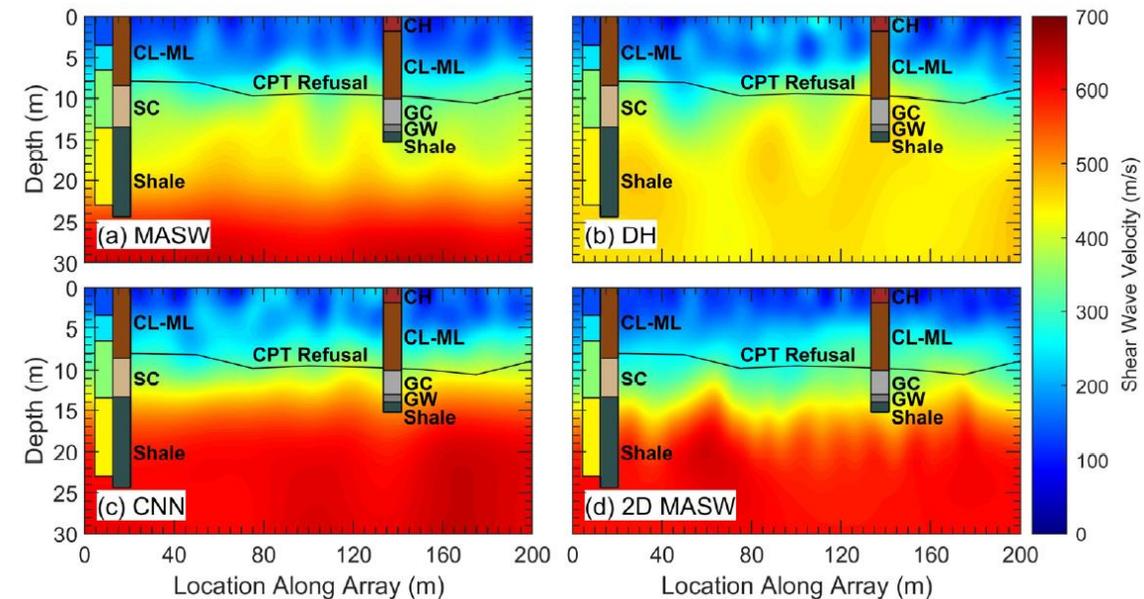
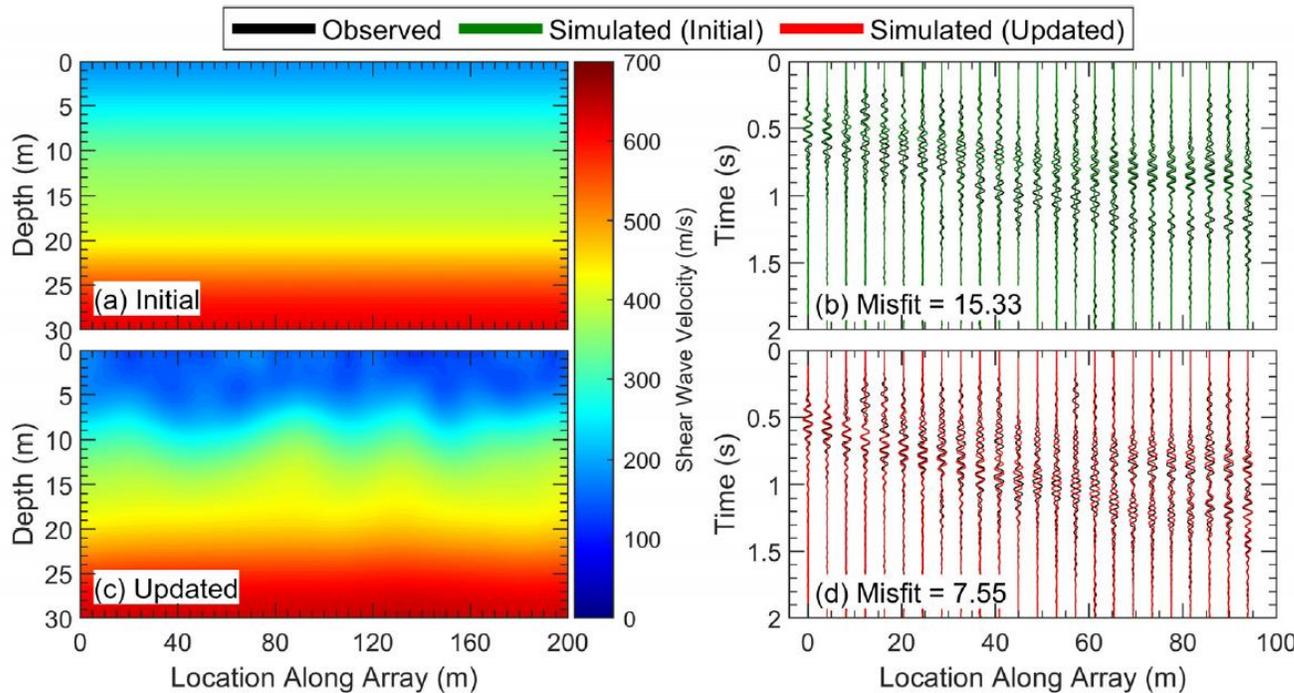


Future Work on This Dataset

- 2D imaging of the ECZ and the SSAF to retrieve Vs and D via:
 - Pseudo-2D MASW
 - Full waveform inversion (FWI)

Near-Surface 2D Imaging via FWI of DAS Data: An Examination on the Impacts of FWI Starting Model

Michael B. S. Yust^{1,*}, Brady R. Cox^{2,*}, Joseph P. Vantassel³, Peter G. Hubbard⁴, Christian Boehm⁵ and Lion Krischer⁵



Sorry... No Time to Talk About Damping

Papers Published on Extracting Damping from Surface Wave Methods

- Abbas, A., Aimar, M., Cox, B.R., Foti, S. (2025). "A Frequency-Domain Beamforming Procedure for Extracting Rayleigh Wave Attenuation Coefficients and Small-Strain Damping Ratio from 2D Ambient Noise Array Measurements," *Earthquake Spectra* 0 (0). (<https://doi.org/10.1177/87552930241304914>).
- Aimar, M., Foti, S., Cox, B.R. (2024a). "Novel Techniques for In-situ Estimation of Shear-wave Velocity and Damping Ratio through MASW testing Part I: A Beamforming Procedure for Extracting Rayleigh-wave Phase Velocity and Phase Attenuation," *Geophysics Journal International* 237 (1): 506 – 524. (<https://doi.org/10.1093/gji/ggae051>).
- Aimar, M., Foti, S., Cox, B.R. (2024b). "Novel Techniques for In-situ Estimation of Shear-wave Velocity and Damping Ratio through MASW testing Part II: A Monte Carlo Algorithm for the Joint Inversion of Phase Velocity and Attenuation," *Geophysics Journal International* 237 (1): 525 – 539. (<https://doi.org/10.1093/gji/ggae050>).
- Abbas, A., Aimar, M., Yust, M., Cox, B.R., Foti, S. (2024). "Emerging Technologies and Advanced Analyses for Non-invasive Near-surface Site Characterization," *Soil and Rocks* 47(3): e2024006923. (<https://www.soilsandrocks.com/issue/68>).
- Aimar, M., Cox, B.R., Foti, S. (2023). "Surface Wave Testing with Distributed Acoustic Sensing Measurements to Estimate the Shear-Wave Velocity and the Small-Strain Damping Ratio," National Conference of the Researchers of Geotechnical Engineering (CNRIG'23), Palermo, Italy, 5-7 July 2023.
- Aimar, M., Francavilla, M., Cox, B.R., Foti, S. (2022). "In-situ characterization of the near-surface small strain damping ratio at the Garner Valley Downhole Array through surface waves analysis," 4th International Conference on Performance-based Design in Earthquake Geotechnical Engineering, Beijing, China, 15-17 July 2022.

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Questions?